

**LANDFILL GAS COLLECTION
SYSTEM DESIGN CALCULATIONS**

WASHINGTON RENEWABLE ENERGY, LLC
FORTY WEST LANDFILL
HAGERSTOWN, MARYLAND

Prepared for
Washington Renewable Energy, LLC

February 2010



1375 Euclid Avenue, Suite 600
Cleveland, Ohio 44115
Project No. 13813514

Stage I
Cells 1 through Cell 4
LandGEM Calculations

JOB Forty West Landfill, Cells 1-4
DESCRIPTION Mueller Equation Calcs

PROJECT NO. 13813514.00001
COMPUTED BY KMC
CHECKED BY NSG/JDM

DATE: 01 Dec 2009
DATE: 18 Jan 2010

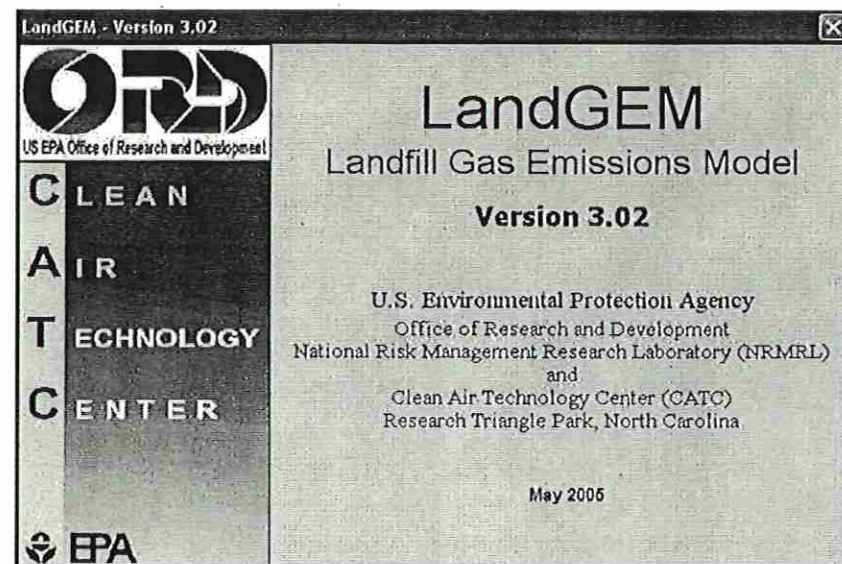
7 The accumulated condensate production is calculated by using Antoine's Equation.

$$V_{(cond)} = \frac{5,694 \times 10^6}{P_s}$$
$$\beta = 6.32 - \frac{3,081}{T + 385}$$

The volume produced per million cubic foot of LFG calculated by Antoine's Equation is then multiplied by the flow of LFG to find the rate of condensate produced. Where P_s = system pressure in psia and T = temperature of the landfill gas within the header system in °F.

8 Using Manning's Formula for gravity flow, solve for the depth of the condensate based on the pipe's slope, pipe size, and flow.

9 The worst case lateral was taken to be the farthest well from the blower that was expected to have the largest headloss. After an evaluation of the plan drawings, well HW-4-1 was chosen to be the worst case lateral.



Summary Report

Landfill Name or Identifier: Forty West Landfill--Cells 1 - 4

Date: Friday, February 19, 2010

Description/Comments:

*Assuming 1% annual waste placement increase after 2008.

**Capacity of Cells 1-4 is 4,047,000 cubic yards. At an effective density of 0.60 tons/cubic yard, yields 2,428,200 short tons.

About LandGEM:

First-Order Decomposition Rate Equation:
$$Q_{CH_4} = \sum_{i=1}^n \sum_{j=0.1}^1 kL_o \left(\frac{M_i}{10} \right) e^{-kt_{ij}}$$

Where,

Q_{CH_4} = annual methane generation in the year of the calculation ($m^3/year$)

i = 1-year time increment

n = (year of the calculation) - (initial year of waste acceptance)

j = 0.1-year time increment

k = methane generation rate ($year^{-1}$)

L_o = potential methane generation capacity (m^3/Mg)

M_i = mass of waste accepted in the i^{th} year (Mg)

t_{ij} = age of the j^{th} section of waste mass M_i accepted in the i^{th} year (decimal years, e.g., 3.2 years)

LandGEM is based on a first-order decomposition rate equation for quantifying emissions from the decomposition of landfilled waste in municipal solid waste (MSW) landfills. The software provides a relatively simple approach to estimating landfill gas emissions. Model defaults are based on empirical data from U.S. landfills. Field test data can also be used in place of model defaults when available. Further guidance on EPA test methods, Clean Air Act (CAA) regulations, and other guidance regarding landfill gas emissions and control technology requirements can be found at <http://www.epa.gov/ttnatw01/landfill/landflpg.html>.

LandGEM is considered a screening tool — the better the input data, the better the estimates. Often, there are limitations with the available data regarding waste quantity and composition, variation in design and operating practices over time, and changes occurring over time that impact the emissions potential. Changes to landfill operation, such as operating under wet conditions through leachate recirculation or other liquid additions, will result in generating more gas at a faster rate. Defaults for estimating emissions for this type of operation are being developed to include in LandGEM along with defaults for conventional landfills (no leachate or liquid additions) for developing emission inventories and determining CAA applicability. Refer to the Web site identified above for future updates.

Input Review

LANDFILL CHARACTERISTICS

| | | |
|--|-----------|------------|
| Landfill Open Year | 2000 | |
| Landfill Closure Year (with 80-year limit) | 2018 | |
| Actual Closure Year (without limit) | 2018 | |
| Have Model Calculate Closure Year? | Yes | |
| Waste Design Capacity | 2,428,200 | short tons |

MODEL PARAMETERS

| | | |
|---|-------|--------------------|
| Methane Generation Rate, k | 0.040 | year ⁻¹ |
| Potential Methane Generation Capacity, L ₀ | 100 | m ³ /Mg |
| NMOC Concentration | 109 | ppmv as hexane |
| Methane Content | 50 | % by volume |

GASES / POLLUTANTS SELECTED

| | |
|---------------------|--------------------|
| Gas / Pollutant #1: | Total landfill gas |
| Gas / Pollutant #2: | Methane |
| Gas / Pollutant #3: | Carbon dioxide |
| Gas / Pollutant #4: | NMOC |

WASTE ACCEPTANCE RATES

| Year | Waste Accepted | | Waste-In-Place | |
|------|----------------|-------------------|----------------|--------------|
| | (Mg/year) | (short tons/year) | (Mg) | (short tons) |
| 2000 | 1,818 | 2,000 | 0 | 0 |
| 2001 | 92,454 | 101,699 | 1,818 | 2,000 |
| 2002 | 108,285 | 119,113 | 94,272 | 103,699 |
| 2003 | 119,441 | 131,385 | 202,556 | 222,812 |
| 2004 | 136,451 | 150,096 | 321,997 | 354,197 |
| 2005 | 158,062 | 173,868 | 458,448 | 504,293 |
| 2006 | 141,335 | 155,468 | 616,510 | 678,161 |
| 2007 | 121,698 | 133,868 | 757,845 | 833,629 |
| 2008 | 120,305 | 132,336 | 879,543 | 967,497 |
| 2009 | 121,509 | 133,659 | 999,848 | 1,099,833 |
| 2010 | 122,724 | 134,996 | 1,121,357 | 1,233,492 |
| 2011 | 123,951 | 136,346 | 1,244,080 | 1,368,488 |
| 2012 | 125,190 | 137,709 | 1,368,031 | 1,504,834 |
| 2013 | 126,442 | 139,086 | 1,493,221 | 1,642,544 |
| 2014 | 127,707 | 140,477 | 1,619,664 | 1,781,630 |
| 2015 | 128,984 | 141,882 | 1,747,370 | 1,922,107 |
| 2016 | 130,274 | 143,301 | 1,876,354 | 2,063,989 |
| 2017 | 131,576 | 144,734 | 2,006,628 | 2,207,290 |
| 2018 | 69,251 | 76,176 | 2,138,204 | 2,352,024 |
| 2019 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2020 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2021 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2022 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2023 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2024 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2025 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2026 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2027 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2028 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2029 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2030 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2031 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2032 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2033 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2034 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2035 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2036 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2037 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2038 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2039 | 0 | 0 | 2,207,455 | 2,428,200 |

WASTE ACCEPTANCE RATES (Continued)

| Year | Waste Accepted | | Waste-In-Place | |
|------|----------------|-------------------|----------------|--------------|
| | (Mg/year) | (short tons/year) | (Mg) | (short tons) |
| 2040 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2041 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2042 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2043 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2044 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2045 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2046 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2047 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2048 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2049 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2050 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2051 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2052 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2053 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2054 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2055 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2056 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2057 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2058 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2059 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2060 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2061 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2062 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2063 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2064 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2065 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2066 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2067 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2068 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2069 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2070 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2071 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2072 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2073 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2074 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2075 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2076 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2077 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2078 | 0 | 0 | 2,207,455 | 2,428,200 |
| 2079 | 0 | 0 | 2,207,455 | 2,428,200 |

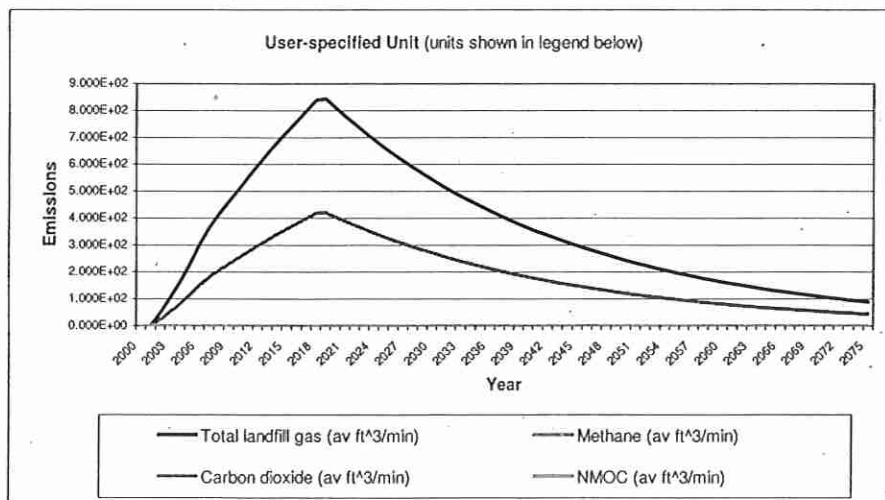
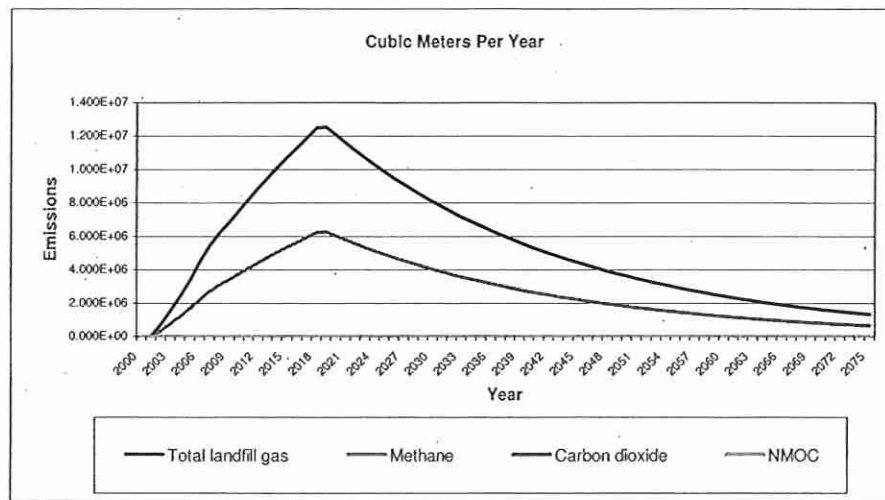
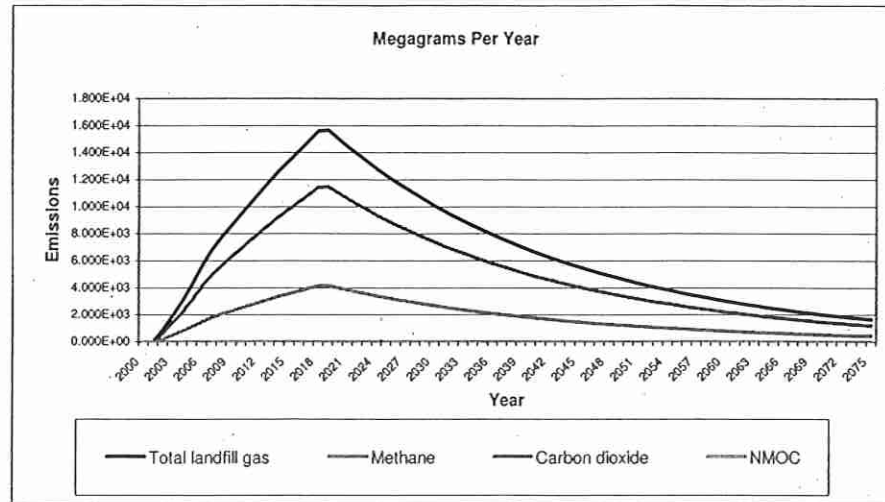
Pollutant Parameters

| <i>Gas / Pollutant Default Parameters:</i> | | | | <i>User-specified Pollutant Parameters:</i> | |
|--|--|-------------------------|------------------|---|------------------|
| | Compound | Concentration (ppmv) | Molecular Weight | Concentration (ppmv) | Molecular Weight |
| Gases | Total landfill gas | | 0.00 | | |
| | Methane | | 16.04 | | |
| | Carbon dioxide | | 44.01 | | |
| | NMOC | 4,000 | 86.18 | | |
| Pollutants | 1,1,1-Trichloroethane (methyl chloroform) - HAP | 0.48 | 133.41 | | |
| | 1,1,2,2- Tetrachloroethane - - HAP/VOC | 1.1 | 167.85 | | |
| | 1,1-Dichloroethane (ethylidene dichloride) - HAP/VOC | 2.4 | 98.97 | | |
| | 1,1-Dichloroethene (vinylidene chloride) - HAP/VOC | 0.20 | 96.94 | | |
| | 1,2-Dichloroethane (ethylene dichloride) - HAP/VOC | 0.41 | 98.96 | | |
| | 1,2-Dichloropropane (propylene dichloride) - HAP/VOC | 0.18 | 112.99 | | |
| | 2-Propanol (isopropyl alcohol) - VOC | 50 | 60.11 | | |
| | Acetone | 7.0 | 58.08 | | |
| | Acrylonitrile - HAP/VOC | 6.3 | 53.06 | | |
| | Benzene - No or Unknown Co-disposal - HAP/VOC | 1.9 | 78.11 | | |
| | Benzene - Co-disposal - HAP/VOC | 11 | 78.11 | | |
| | Bromodichloromethane - VOC | 3.1 | 163.83 | | |
| | Butane - VOC | 5.0 | 58.12 | | |
| | Carbon disulfide - HAP/VOC | 0.58 | 76.13 | | |
| | Carbon monoxide | 140 | 28.01 | | |
| | Carbon tetrachloride - HAP/VOC | 4.0E-03 | 153.84 | | |
| | Carbonyl sulfide - HAP/VOC | 0.49 | 60.07 | | |
| | Chlorobenzene - HAP/VOC | 0.25 | 112.56 | | |
| | Chlorodifluoromethane | 1.3 | 86.47 | | |
| | Chloroethane (ethyl chloride) - HAP/VOC | 1.3 | 64.52 | | |
| | Chloroform - HAP/VOC | 0.03 | 119.39 | | |
| | Chloromethane - VOC | 1.2 | 50.49 | | |
| | Dichlorobenzene - (HAP for para isomer/VOC) | 0.21 | 147 | | |
| | Dichlorodifluoromethane | 16 | 120.91 | | |
| | Dichlorofluoromethane - VOC | 2.6 | 102.92 | | |
| | Dichloromethane (methylene chloride) - HAP | 14 | 84.94 | | |
| | Dimethyl sulfide (methyl sulfide) - VOC | 7.8 | 62.13 | | |
| | Ethane | 890 | 30.07 | | |
| | Ethanol - VOC | 27 | 46.08 | | |

Pollutant Parameters (Continued)

| | | <i>Gas / Pollutant Default Parameters:</i> | | <i>User-specified Pollutant Parameters:</i> | |
|------------|---|--|------------------|---|------------------|
| | | Concentration (ppmv) | Molecular Weight | Concentration (ppmv) | Molecular Weight |
| Pollutants | Ethyl mercaptan (ethanethiol) - VOC | 2.3 | 62.13 | | |
| | Ethylbenzene - HAP/VOC | 4.6 | 106.16 | | |
| | Ethylene dibromide - HAP/VOC | 1.0E-03 | 187.88 | | |
| | Fluorotrichloromethane - VOC | 0.76 | 137.38 | | |
| | Hexane - HAP/VOC | 6.6 | 86.18 | | |
| | Hydrogen sulfide | 36 | 34.08 | | |
| | Mercury (total) - HAP | 2.9E-04 | 200.61 | | |
| | Methyl ethyl ketone - HAP/VOC | 7.1 | 72.11 | | |
| | Methyl isobutyl ketone - HAP/VOC | 1.9 | 100.16 | | |
| | Methyl mercaptan - VOC | 2.5 | 48.11 | | |
| | Pentane - VOC | 3.3 | 72.15 | | |
| | Perchloroethylene (tetrachloroethylene) - HAP | 3.7 | 165.83 | | |
| | Propane - VOC | 11 | 44.09 | | |
| | t-1,2-Dichloroethene - VOC | 2.8 | 96.94 | | |
| | Toluene - No or Unknown Co-disposal - HAP/VOC | 39 | 92.13 | | |
| | Toluene - Co-disposal - HAP/VOC | 170 | 92.13 | | |
| | Trichloroethylene (trichloroethene) - HAP/VOC | 2.8 | 131.40 | | |
| | Vinyl chloride - HAP/VOC | 7.3 | 62.50 | | |
| | Xylenes - HAP/VOC | 12 | 106.16 | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

Graphs



Results

| Year | Total landfill gas | | | Methane | | |
|------|--------------------|------------------------|---------------------------|-----------|------------------------|---------------------------|
| | (Mg/year) | (m ³ /year) | (av ft ³ /min) | (Mg/year) | (m ³ /year) | (av ft ³ /min) |
| 2000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2001 | 1.784E+01 | 1.429E+04 | 9.599E-01 | 4.766E+00 | 7.143E+03 | 4.800E-01 |
| 2002 | 9.244E+02 | 7.402E+05 | 4.973E+01 | 2.469E+02 | 3.701E+05 | 2.487E+01 |
| 2003 | 1.951E+03 | 1.562E+06 | 1.050E+02 | 5.211E+02 | 7.810E+05 | 5.248E+01 |
| 2004 | 3.046E+03 | 2.439E+06 | 1.639E+02 | 8.137E+02 | 1.220E+06 | 8.195E+01 |
| 2005 | 4.266E+03 | 3.416E+06 | 2.295E+02 | 1.139E+03 | 1.708E+06 | 1.148E+02 |
| 2006 | 5.650E+03 | 4.524E+06 | 3.040E+02 | 1.509E+03 | 2.262E+06 | 1.520E+02 |
| 2007 | 6.815E+03 | 5.457E+06 | 3.667E+02 | 1.820E+03 | 2.729E+06 | 1.833E+02 |
| 2008 | 7.742E+03 | 6.199E+06 | 4.165E+02 | 2.068E+03 | 3.100E+06 | 2.083E+02 |
| 2009 | 8.619E+03 | 6.902E+06 | 4.637E+02 | 2.302E+03 | 3.451E+06 | 2.319E+02 |
| 2010 | 9.473E+03 | 7.586E+06 | 5.097E+02 | 2.530E+03 | 3.793E+06 | 2.548E+02 |
| 2011 | 1.031E+04 | 8.253E+06 | 5.545E+02 | 2.753E+03 | 4.126E+06 | 2.773E+02 |
| 2012 | 1.112E+04 | 8.903E+06 | 5.982E+02 | 2.970E+03 | 4.452E+06 | 2.991E+02 |
| 2013 | 1.191E+04 | 9.538E+06 | 6.408E+02 | 3.182E+03 | 4.769E+06 | 3.204E+02 |
| 2014 | 1.268E+04 | 1.016E+07 | 6.825E+02 | 3.388E+03 | 5.079E+06 | 3.412E+02 |
| 2015 | 1.344E+04 | 1.076E+07 | 7.231E+02 | 3.590E+03 | 5.381E+06 | 3.616E+02 |
| 2016 | 1.418E+04 | 1.135E+07 | 7.629E+02 | 3.787E+03 | 5.677E+06 | 3.814E+02 |
| 2017 | 1.490E+04 | 1.193E+07 | 8.017E+02 | 3.980E+03 | 5.966E+06 | 4.009E+02 |
| 2018 | 1.561E+04 | 1.250E+07 | 8.398E+02 | 4.169E+03 | 6.249E+06 | 4.199E+02 |
| 2019 | 1.568E+04 | 1.255E+07 | 8.434E+02 | 4.187E+03 | 6.276E+06 | 4.217E+02 |
| 2020 | 1.506E+04 | 1.206E+07 | 8.103E+02 | 4.023E+03 | 6.030E+06 | 4.052E+02 |
| 2021 | 1.447E+04 | 1.159E+07 | 7.786E+02 | 3.865E+03 | 5.794E+06 | 3.893E+02 |
| 2022 | 1.390E+04 | 1.113E+07 | 7.480E+02 | 3.714E+03 | 5.567E+06 | 3.740E+02 |
| 2023 | 1.336E+04 | 1.070E+07 | 7.187E+02 | 3.568E+03 | 5.348E+06 | 3.594E+02 |
| 2024 | 1.283E+04 | 1.028E+07 | 6.905E+02 | 3.428E+03 | 5.139E+06 | 3.453E+02 |
| 2025 | 1.233E+04 | 9.874E+06 | 6.635E+02 | 3.294E+03 | 4.937E+06 | 3.317E+02 |
| 2026 | 1.185E+04 | 9.487E+06 | 6.374E+02 | 3.165E+03 | 4.744E+06 | 3.187E+02 |
| 2027 | 1.138E+04 | 9.115E+06 | 6.124E+02 | 3.041E+03 | 4.558E+06 | 3.062E+02 |
| 2028 | 1.094E+04 | 8.758E+06 | 5.884E+02 | 2.921E+03 | 4.379E+06 | 2.942E+02 |
| 2029 | 1.051E+04 | 8.414E+06 | 5.654E+02 | 2.807E+03 | 4.207E+06 | 2.827E+02 |
| 2030 | 1.010E+04 | 8.084E+06 | 5.432E+02 | 2.697E+03 | 4.042E+06 | 2.716E+02 |
| 2031 | 9.700E+03 | 7.767E+06 | 5.219E+02 | 2.591E+03 | 3.884E+06 | 2.609E+02 |
| 2032 | 9.320E+03 | 7.463E+06 | 5.014E+02 | 2.489E+03 | 3.731E+06 | 2.507E+02 |
| 2033 | 8.954E+03 | 7.170E+06 | 4.818E+02 | 2.392E+03 | 3.585E+06 | 2.409E+02 |
| 2034 | 8.603E+03 | 6.889E+06 | 4.629E+02 | 2.298E+03 | 3.445E+06 | 2.314E+02 |
| 2035 | 8.266E+03 | 6.619E+06 | 4.447E+02 | 2.208E+03 | 3.309E+06 | 2.224E+02 |
| 2036 | 7.942E+03 | 6.359E+06 | 4.273E+02 | 2.121E+03 | 3.180E+06 | 2.136E+02 |
| 2037 | 7.630E+03 | 6.110E+06 | 4.105E+02 | 2.038E+03 | 3.055E+06 | 2.053E+02 |
| 2038 | 7.331E+03 | 5.870E+06 | 3.944E+02 | 1.958E+03 | 2.935E+06 | 1.972E+02 |
| 2039 | 7.044E+03 | 5.640E+06 | 3.790E+02 | 1.881E+03 | 2.820E+06 | 1.895E+02 |
| 2040 | 6.768E+03 | 5.419E+06 | 3.641E+02 | 1.808E+03 | 2.710E+06 | 1.821E+02 |
| 2041 | 6.502E+03 | 5.207E+06 | 3.498E+02 | 1.737E+03 | 2.603E+06 | 1.749E+02 |
| 2042 | 6.247E+03 | 5.002E+06 | 3.361E+02 | 1.669E+03 | 2.501E+06 | 1.681E+02 |
| 2043 | 6.002E+03 | 4.806E+06 | 3.229E+02 | 1.603E+03 | 2.403E+06 | 1.615E+02 |
| 2044 | 5.767E+03 | 4.618E+06 | 3.103E+02 | 1.540E+03 | 2.309E+06 | 1.551E+02 |
| 2045 | 5.541E+03 | 4.437E+06 | 2.981E+02 | 1.480E+03 | 2.218E+06 | 1.491E+02 |
| 2046 | 5.324E+03 | 4.263E+06 | 2.864E+02 | 1.422E+03 | 2.131E+06 | 1.432E+02 |
| 2047 | 5.115E+03 | 4.096E+06 | 2.752E+02 | 1.366E+03 | 2.048E+06 | 1.376E+02 |
| 2048 | 4.914E+03 | 3.935E+06 | 2.644E+02 | 1.313E+03 | 1.968E+06 | 1.322E+02 |
| 2049 | 4.722E+03 | 3.781E+06 | 2.540E+02 | 1.261E+03 | 1.890E+06 | 1.270E+02 |

Results (Continued)

| Year | Total landfill gas | | | Methane | | |
|------|--------------------|------------------------|---------------------------|-----------|------------------------|---------------------------|
| | (Mg/year) | (m ³ /year) | (av ft ³ /min) | (Mg/year) | (m ³ /year) | (av ft ³ /min) |
| 2050 | 4.536E+03 | 3.633E+06 | 2.441E+02 | 1.212E+03 | 1.816E+06 | 1.220E+02 |
| 2051 | 4.359E+03 | 3.490E+06 | 2.345E+02 | 1.164E+03 | 1.745E+06 | 1.173E+02 |
| 2052 | 4.188E+03 | 3.353E+06 | 2.253E+02 | 1.119E+03 | 1.677E+06 | 1.127E+02 |
| 2053 | 4.023E+03 | 3.222E+06 | 2.165E+02 | 1.075E+03 | 1.611E+06 | 1.082E+02 |
| 2054 | 3.866E+03 | 3.095E+06 | 2.080E+02 | 1.033E+03 | 1.548E+06 | 1.040E+02 |
| 2055 | 3.714E+03 | 2.974E+06 | 1.998E+02 | 9.921E+02 | 1.487E+06 | 9.991E+01 |
| 2056 | 3.568E+03 | 2.857E+06 | 1.920E+02 | 9.532E+02 | 1.429E+06 | 9.600E+01 |
| 2057 | 3.429E+03 | 2.745E+06 | 1.845E+02 | 9.158E+02 | 1.373E+06 | 9.223E+01 |
| 2058 | 3.294E+03 | 2.638E+06 | 1.772E+02 | 8.799E+02 | 1.319E+06 | 8.862E+01 |
| 2059 | 3.165E+03 | 2.534E+06 | 1.703E+02 | 8.454E+02 | 1.267E+06 | 8.514E+01 |
| 2060 | 3.041E+03 | 2.435E+06 | 1.636E+02 | 8.122E+02 | 1.217E+06 | 8.180E+01 |
| 2061 | 2.922E+03 | 2.339E+06 | 1.572E+02 | 7.804E+02 | 1.170E+06 | 7.860E+01 |
| 2062 | 2.807E+03 | 2.248E+06 | 1.510E+02 | 7.498E+02 | 1.124E+06 | 7.551E+01 |
| 2063 | 2.697E+03 | 2.160E+06 | 1.451E+02 | 7.204E+02 | 1.080E+06 | 7.255E+01 |
| 2064 | 2.591E+03 | 2.075E+06 | 1.394E+02 | 6.921E+02 | 1.037E+06 | 6.971E+01 |
| 2065 | 2.490E+03 | 1.994E+06 | 1.339E+02 | 6.650E+02 | 9.968E+05 | 6.697E+01 |
| 2066 | 2.392E+03 | 1.915E+06 | 1.287E+02 | 6.389E+02 | 9.577E+05 | 6.435E+01 |
| 2067 | 2.298E+03 | 1.840E+06 | 1.237E+02 | 6.139E+02 | 9.202E+05 | 6.183E+01 |
| 2068 | 2.208E+03 | 1.768E+06 | 1.188E+02 | 5.898E+02 | 8.841E+05 | 5.940E+01 |
| 2069 | 2.122E+03 | 1.699E+06 | 1.141E+02 | 5.667E+02 | 8.494E+05 | 5.707E+01 |
| 2070 | 2.038E+03 | 1.632E+06 | 1.097E+02 | 5.445E+02 | 8.161E+05 | 5.483E+01 |
| 2071 | 1.958E+03 | 1.568E+06 | 1.054E+02 | 5.231E+02 | 7.841E+05 | 5.268E+01 |
| 2072 | 1.882E+03 | 1.507E+06 | 1.012E+02 | 5.026E+02 | 7.534E+05 | 5.062E+01 |
| 2073 | 1.808E+03 | 1.448E+06 | 9.727E+01 | 4.829E+02 | 7.238E+05 | 4.863E+01 |
| 2074 | 1.737E+03 | 1.391E+06 | 9.345E+01 | 4.640E+02 | 6.954E+05 | 4.673E+01 |
| 2075 | 1.669E+03 | 1.336E+06 | 8.979E+01 | 4.458E+02 | 6.682E+05 | 4.489E+01 |
| 2076 | 1.603E+03 | 1.284E+06 | 8.627E+01 | 4.283E+02 | 6.420E+05 | 4.313E+01 |
| 2077 | 1.541E+03 | 1.234E+06 | 8.289E+01 | 4.115E+02 | 6.168E+05 | 4.144E+01 |
| 2078 | 1.480E+03 | 1.185E+06 | 7.964E+01 | 3.954E+02 | 5.926E+05 | 3.982E+01 |
| 2079 | 1.422E+03 | 1.139E+06 | 7.651E+01 | 3.799E+02 | 5.694E+05 | 3.826E+01 |
| 2080 | 1.366E+03 | 1.094E+06 | 7.351E+01 | 3.650E+02 | 5.471E+05 | 3.676E+01 |
| 2081 | 1.313E+03 | 1.051E+06 | 7.063E+01 | 3.507E+02 | 5.256E+05 | 3.532E+01 |
| 2082 | 1.261E+03 | 1.010E+06 | 6.786E+01 | 3.369E+02 | 5.050E+05 | 3.393E+01 |
| 2083 | 1.212E+03 | 9.704E+05 | 6.520E+01 | 3.237E+02 | 4.852E+05 | 3.260E+01 |
| 2084 | 1.164E+03 | 9.323E+05 | 6.264E+01 | 3.110E+02 | 4.662E+05 | 3.132E+01 |
| 2085 | 1.119E+03 | 8.958E+05 | 6.019E+01 | 2.988E+02 | 4.479E+05 | 3.009E+01 |
| 2086 | 1.075E+03 | 8.607E+05 | 5.783E+01 | 2.871E+02 | 4.303E+05 | 2.891E+01 |
| 2087 | 1.033E+03 | 8.269E+05 | 5.556E+01 | 2.758E+02 | 4.135E+05 | 2.778E+01 |
| 2088 | 9.922E+02 | 7.945E+05 | 5.338E+01 | 2.650E+02 | 3.972E+05 | 2.669E+01 |
| 2089 | 9.533E+02 | 7.633E+05 | 5.129E+01 | 2.546E+02 | 3.817E+05 | 2.564E+01 |
| 2090 | 9.159E+02 | 7.334E+05 | 4.928E+01 | 2.446E+02 | 3.667E+05 | 2.464E+01 |
| 2091 | 8.800E+02 | 7.046E+05 | 4.734E+01 | 2.351E+02 | 3.523E+05 | 2.367E+01 |
| 2092 | 8.455E+02 | 6.770E+05 | 4.549E+01 | 2.258E+02 | 3.385E+05 | 2.274E+01 |
| 2093 | 8.123E+02 | 6.505E+05 | 4.370E+01 | 2.170E+02 | 3.252E+05 | 2.185E+01 |
| 2094 | 7.805E+02 | 6.250E+05 | 4.199E+01 | 2.085E+02 | 3.125E+05 | 2.100E+01 |
| 2095 | 7.499E+02 | 6.005E+05 | 4.034E+01 | 2.003E+02 | 3.002E+05 | 2.017E+01 |
| 2096 | 7.205E+02 | 5.769E+05 | 3.876E+01 | 1.924E+02 | 2.885E+05 | 1.938E+01 |
| 2097 | 6.922E+02 | 5.543E+05 | 3.724E+01 | 1.849E+02 | 2.771E+05 | 1.862E+01 |
| 2098 | 6.651E+02 | 5.326E+05 | 3.578E+01 | 1.776E+02 | 2.663E+05 | 1.789E+01 |
| 2099 | 6.390E+02 | 5.117E+05 | 3.438E+01 | 1.707E+02 | 2.558E+05 | 1.719E+01 |
| 2100 | 6.139E+02 | 4.916E+05 | 3.303E+01 | 1.640E+02 | 2.458E+05 | 1.652E+01 |

Results (Continued)

| Year | Total landfill gas | | | Methane | | |
|------|--------------------|------------------------|---------------------------|-----------|------------------------|---------------------------|
| | (Mg/year) | (m ³ /year) | (av ft ³ /min) | (Mg/year) | (m ³ /year) | (av ft ³ /min) |
| 2101 | 5.899E+02 | 4.723E+05 | 3.174E+01 | 1.576E+02 | 2.362E+05 | 1.587E+01 |
| 2102 | 5.667E+02 | 4.538E+05 | 3.049E+01 | 1.514E+02 | 2.269E+05 | 1.525E+01 |
| 2103 | 5.445E+02 | 4.360E+05 | 2.930E+01 | 1.454E+02 | 2.180E+05 | 1.465E+01 |
| 2104 | 5.232E+02 | 4.189E+05 | 2.815E+01 | 1.397E+02 | 2.095E+05 | 1.407E+01 |
| 2105 | 5.026E+02 | 4.025E+05 | 2.704E+01 | 1.343E+02 | 2.012E+05 | 1.352E+01 |
| 2106 | 4.829E+02 | 3.867E+05 | 2.598E+01 | 1.290E+02 | 1.934E+05 | 1.299E+01 |
| 2107 | 4.640E+02 | 3.716E+05 | 2.496E+01 | 1.239E+02 | 1.858E+05 | 1.248E+01 |
| 2108 | 4.458E+02 | 3.570E+05 | 2.399E+01 | 1.191E+02 | 1.785E+05 | 1.199E+01 |
| 2109 | 4.283E+02 | 3.430E+05 | 2.305E+01 | 1.144E+02 | 1.715E+05 | 1.152E+01 |
| 2110 | 4.115E+02 | 3.295E+05 | 2.214E+01 | 1.099E+02 | 1.648E+05 | 1.107E+01 |
| 2111 | 3.954E+02 | 3.166E+05 | 2.127E+01 | 1.056E+02 | 1.583E+05 | 1.064E+01 |
| 2112 | 3.799E+02 | 3.042E+05 | 2.044E+01 | 1.015E+02 | 1.521E+05 | 1.022E+01 |
| 2113 | 3.650E+02 | 2.923E+05 | 1.964E+01 | 9.749E+01 | 1.461E+05 | 9.819E+00 |
| 2114 | 3.507E+02 | 2.808E+05 | 1.887E+01 | 9.367E+01 | 1.404E+05 | 9.434E+00 |
| 2115 | 3.369E+02 | 2.698E+05 | 1.813E+01 | 9.000E+01 | 1.349E+05 | 9.064E+00 |
| 2116 | 3.237E+02 | 2.592E+05 | 1.742E+01 | 8.647E+01 | 1.296E+05 | 8.709E+00 |
| 2117 | 3.110E+02 | 2.491E+05 | 1.673E+01 | 8.308E+01 | 1.245E+05 | 8.367E+00 |
| 2118 | 2.988E+02 | 2.393E+05 | 1.608E+01 | 7.982E+01 | 1.196E+05 | 8.039E+00 |
| 2119 | 2.871E+02 | 2.299E+05 | 1.545E+01 | 7.669E+01 | 1.150E+05 | 7.724E+00 |
| 2120 | 2.759E+02 | 2.209E+05 | 1.484E+01 | 7.369E+01 | 1.104E+05 | 7.421E+00 |
| 2121 | 2.650E+02 | 2.122E+05 | 1.426E+01 | 7.080E+01 | 1.061E+05 | 7.130E+00 |
| 2122 | 2.547E+02 | 2.039E+05 | 1.370E+01 | 6.802E+01 | 1.020E+05 | 6.850E+00 |
| 2123 | 2.447E+02 | 1.959E+05 | 1.316E+01 | 6.535E+01 | 9.796E+04 | 6.582E+00 |
| 2124 | 2.351E+02 | 1.882E+05 | 1.265E+01 | 6.279E+01 | 9.412E+04 | 6.324E+00 |
| 2125 | 2.259E+02 | 1.809E+05 | 1.215E+01 | 6.033E+01 | 9.043E+04 | 6.076E+00 |
| 2126 | 2.170E+02 | 1.738E+05 | 1.168E+01 | 5.796E+01 | 8.688E+04 | 5.838E+00 |
| 2127 | 2.085E+02 | 1.669E+05 | 1.122E+01 | 5.569E+01 | 8.347E+04 | 5.609E+00 |
| 2128 | 2.003E+02 | 1.604E+05 | 1.078E+01 | 5.351E+01 | 8.020E+04 | 5.389E+00 |
| 2129 | 1.925E+02 | 1.541E+05 | 1.035E+01 | 5.141E+01 | 7.706E+04 | 5.177E+00 |
| 2130 | 1.849E+02 | 1.481E+05 | 9.949E+00 | 4.939E+01 | 7.404E+04 | 4.974E+00 |
| 2131 | 1.777E+02 | 1.423E+05 | 9.559E+00 | 4.746E+01 | 7.113E+04 | 4.779E+00 |
| 2132 | 1.707E+02 | 1.367E+05 | 9.184E+00 | 4.560E+01 | 6.834E+04 | 4.592E+00 |
| 2133 | 1.640E+02 | 1.313E+05 | 8.824E+00 | 4.381E+01 | 6.566E+04 | 4.412E+00 |
| 2134 | 1.576E+02 | 1.262E+05 | 8.478E+00 | 4.209E+01 | 6.309E+04 | 4.239E+00 |
| 2135 | 1.514E+02 | 1.212E+05 | 8.145E+00 | 4.044E+01 | 6.062E+04 | 4.073E+00 |
| 2136 | 1.455E+02 | 1.165E+05 | 7.826E+00 | 3.885E+01 | 5.824E+04 | 3.913E+00 |
| 2137 | 1.398E+02 | 1.119E+05 | 7.519E+00 | 3.733E+01 | 5.595E+04 | 3.760E+00 |
| 2138 | 1.343E+02 | 1.075E+05 | 7.224E+00 | 3.587E+01 | 5.376E+04 | 3.612E+00 |
| 2139 | 1.290E+02 | 1.033E+05 | 6.941E+00 | 3.446E+01 | 5.165E+04 | 3.471E+00 |
| 2140 | 1.240E+02 | 9.925E+04 | 6.669E+00 | 3.311E+01 | 4.963E+04 | 3.334E+00 |

Results (Continued)

| Year | Carbon dioxide | | | NMOC | | |
|------|----------------|------------------------|---------------------------|-----------|------------------------|---------------------------|
| | (Mg/year) | (m ³ /year) | (av ft ³ /min) | (Mg/year) | (m ³ /year) | (av ft ³ /min) |
| 2000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2001 | 1.308E+01 | 7.143E+03 | 4.800E-01 | 5.582E-03 | 1.557E+00 | 1.046E-04 |
| 2002 | 6.775E+02 | 3.701E+05 | 2.487E+01 | 2.892E-01 | 8.068E+01 | 5.421E-03 |
| 2003 | 1.430E+03 | 7.810E+05 | 5.248E+01 | 6.103E-01 | 1.703E+02 | 1.144E-02 |
| 2004 | 2.233E+03 | 1.220E+06 | 8.195E+01 | 9.531E-01 | 2.659E+02 | 1.787E-02 |
| 2005 | 3.126E+03 | 1.708E+06 | 1.148E+02 | 1.335E+00 | 3.723E+02 | 2.502E-02 |
| 2006 | 4.141E+03 | 2.262E+06 | 1.520E+02 | 1.768E+00 | 4.931E+02 | 3.313E-02 |
| 2007 | 4.995E+03 | 2.729E+06 | 1.833E+02 | 2.132E+00 | 5.948E+02 | 3.997E-02 |
| 2008 | 5.674E+03 | 3.100E+06 | 2.083E+02 | 2.422E+00 | 6.757E+02 | 4.540E-02 |
| 2009 | 6.317E+03 | 3.451E+06 | 2.319E+02 | 2.697E+00 | 7.523E+02 | 5.055E-02 |
| 2010 | 6.943E+03 | 3.793E+06 | 2.548E+02 | 2.964E+00 | 8.269E+02 | 5.556E-02 |
| 2011 | 7.553E+03 | 4.126E+06 | 2.773E+02 | 3.224E+00 | 8.996E+02 | 6.044E-02 |
| 2012 | 8.149E+03 | 4.452E+06 | 2.991E+02 | 3.479E+00 | 9.704E+02 | 6.520E-02 |
| 2013 | 8.729E+03 | 4.769E+06 | 3.204E+02 | 3.726E+00 | 1.040E+03 | 6.985E-02 |
| 2014 | 9.297E+03 | 5.079E+06 | 3.412E+02 | 3.969E+00 | 1.107E+03 | 7.439E-02 |
| 2015 | 9.850E+03 | 5.381E+06 | 3.616E+02 | 4.205E+00 | 1.173E+03 | 7.882E-02 |
| 2016 | 1.039E+04 | 5.677E+06 | 3.814E+02 | 4.436E+00 | 1.238E+03 | 8.315E-02 |
| 2017 | 1.092E+04 | 5.966E+06 | 4.009E+02 | 4.662E+00 | 1.301E+03 | 8.739E-02 |
| 2018 | 1.144E+04 | 6.249E+06 | 4.199E+02 | 4.883E+00 | 1.362E+03 | 9.154E-02 |
| 2019 | 1.149E+04 | 6.276E+06 | 4.217E+02 | 4.904E+00 | 1.368E+03 | 9.193E-02 |
| 2020 | 1.104E+04 | 6.030E+06 | 4.052E+02 | 4.712E+00 | 1.315E+03 | 8.833E-02 |
| 2021 | 1.061E+04 | 5.794E+06 | 3.893E+02 | 4.527E+00 | 1.263E+03 | 8.486E-02 |
| 2022 | 1.019E+04 | 5.567E+06 | 3.740E+02 | 4.350E+00 | 1.214E+03 | 8.154E-02 |
| 2023 | 9.790E+03 | 5.348E+06 | 3.594E+02 | 4.179E+00 | 1.166E+03 | 7.834E-02 |
| 2024 | 9.406E+03 | 5.139E+06 | 3.453E+02 | 4.015E+00 | 1.120E+03 | 7.527E-02 |
| 2025 | 9.037E+03 | 4.937E+06 | 3.317E+02 | 3.858E+00 | 1.076E+03 | 7.232E-02 |
| 2026 | 8.683E+03 | 4.744E+06 | 3.187E+02 | 3.707E+00 | 1.034E+03 | 6.948E-02 |
| 2027 | 8.343E+03 | 4.558E+06 | 3.062E+02 | 3.561E+00 | 9.935E+02 | 6.676E-02 |
| 2028 | 8.015E+03 | 4.379E+06 | 2.942E+02 | 3.422E+00 | 9.546E+02 | 6.414E-02 |
| 2029 | 7.701E+03 | 4.207E+06 | 2.827E+02 | 3.288E+00 | 9.172E+02 | 6.162E-02 |
| 2030 | 7.399E+03 | 4.042E+06 | 2.716E+02 | 3.159E+00 | 8.812E+02 | 5.921E-02 |
| 2031 | 7.109E+03 | 3.884E+06 | 2.609E+02 | 3.035E+00 | 8.466E+02 | 5.689E-02 |
| 2032 | 6.830E+03 | 3.731E+06 | 2.507E+02 | 2.916E+00 | 8.134E+02 | 5.466E-02 |
| 2033 | 6.563E+03 | 3.585E+06 | 2.409E+02 | 2.801E+00 | 7.816E+02 | 5.251E-02 |
| 2034 | 6.305E+03 | 3.445E+06 | 2.314E+02 | 2.692E+00 | 7.509E+02 | 5.045E-02 |
| 2035 | 6.058E+03 | 3.309E+06 | 2.224E+02 | 2.586E+00 | 7.215E+02 | 4.848E-02 |
| 2036 | 5.820E+03 | 3.180E+06 | 2.136E+02 | 2.485E+00 | 6.932E+02 | 4.657E-02 |
| 2037 | 5.592E+03 | 3.055E+06 | 2.053E+02 | 2.387E+00 | 6.660E+02 | 4.475E-02 |
| 2038 | 5.373E+03 | 2.935E+06 | 1.972E+02 | 2.294E+00 | 6.399E+02 | 4.299E-02 |
| 2039 | 5.162E+03 | 2.820E+06 | 1.895E+02 | 2.204E+00 | 6.148E+02 | 4.131E-02 |
| 2040 | 4.960E+03 | 2.710E+06 | 1.821E+02 | 2.117E+00 | 5.907E+02 | 3.969E-02 |
| 2041 | 4.765E+03 | 2.603E+06 | 1.749E+02 | 2.034E+00 | 5.675E+02 | 3.813E-02 |
| 2042 | 4.579E+03 | 2.501E+06 | 1.681E+02 | 1.955E+00 | 5.453E+02 | 3.664E-02 |
| 2043 | 4.399E+03 | 2.403E+06 | 1.615E+02 | 1.878E+00 | 5.239E+02 | 3.520E-02 |
| 2044 | 4.227E+03 | 2.309E+06 | 1.551E+02 | 1.804E+00 | 5.033E+02 | 3.382E-02 |
| 2045 | 4.061E+03 | 2.218E+06 | 1.491E+02 | 1.733E+00 | 4.836E+02 | 3.249E-02 |
| 2046 | 3.902E+03 | 2.131E+06 | 1.432E+02 | 1.666E+00 | 4.646E+02 | 3.122E-02 |
| 2047 | 3.749E+03 | 2.048E+06 | 1.376E+02 | 1.600E+00 | 4.464E+02 | 3.000E-02 |
| 2048 | 3.602E+03 | 1.968E+06 | 1.322E+02 | 1.537E+00 | 4.289E+02 | 2.882E-02 |
| 2049 | 3.460E+03 | 1.890E+06 | 1.270E+02 | 1.477E+00 | 4.121E+02 | 2.769E-02 |

Results (Continued)

| Year | Carbon dioxide | | | NMOC | | |
|------|----------------|------------------------|---------------------------|-----------|------------------------|---------------------------|
| | (Mg/year) | (m ³ /year) | (av ft ³ /min) | (Mg/year) | (m ³ /year) | (av ft ³ /min) |
| 2050 | 3.325E+03 | 1.816E+06 | 1.220E+02 | 1.419E+00 | 3.959E+02 | 2.660E-02 |
| 2051 | 3.194E+03 | 1.745E+06 | 1.173E+02 | 1.364E+00 | 3.804E+02 | 2.556E-02 |
| 2052 | 3.069E+03 | 1.677E+06 | 1.127E+02 | 1.310E+00 | 3.655E+02 | 2.456E-02 |
| 2053 | 2.949E+03 | 1.611E+06 | 1.082E+02 | 1.259E+00 | 3.512E+02 | 2.360E-02 |
| 2054 | 2.833E+03 | 1.548E+06 | 1.040E+02 | 1.209E+00 | 3.374E+02 | 2.267E-02 |
| 2055 | 2.722E+03 | 1.487E+06 | 9.991E+01 | 1.162E+00 | 3.242E+02 | 2.178E-02 |
| 2056 | 2.615E+03 | 1.429E+06 | 9.600E+01 | 1.116E+00 | 3.115E+02 | 2.093E-02 |
| 2057 | 2.513E+03 | 1.373E+06 | 9.223E+01 | 1.073E+00 | 2.993E+02 | 2.011E-02 |
| 2058 | 2.414E+03 | 1.319E+06 | 8.862E+01 | 1.031E+00 | 2.875E+02 | 1.932E-02 |
| 2059 | 2.320E+03 | 1.267E+06 | 8.514E+01 | 9.902E-01 | 2.762E+02 | 1.856E-02 |
| 2060 | 2.229E+03 | 1.217E+06 | 8.180E+01 | 9.514E-01 | 2.654E+02 | 1.783E-02 |
| 2061 | 2.141E+03 | 1.170E+06 | 7.860E+01 | 9.141E-01 | 2.550E+02 | 1.713E-02 |
| 2062 | 2.057E+03 | 1.124E+06 | 7.551E+01 | 8.782E-01 | 2.450E+02 | 1.646E-02 |
| 2063 | 1.977E+03 | 1.080E+06 | 7.255E+01 | 8.438E-01 | 2.354E+02 | 1.582E-02 |
| 2064 | 1.899E+03 | 1.037E+06 | 6.971E+01 | 8.107E-01 | 2.262E+02 | 1.520E-02 |
| 2065 | 1.825E+03 | 9.968E+05 | 6.697E+01 | 7.789E-01 | 2.173E+02 | 1.460E-02 |
| 2066 | 1.753E+03 | 9.577E+05 | 6.435E+01 | 7.484E-01 | 2.088E+02 | 1.403E-02 |
| 2067 | 1.684E+03 | 9.202E+05 | 6.183E+01 | 7.190E-01 | 2.006E+02 | 1.348E-02 |
| 2068 | 1.618E+03 | 8.841E+05 | 5.940E+01 | 6.908E-01 | 1.927E+02 | 1.295E-02 |
| 2069 | 1.555E+03 | 8.494E+05 | 5.707E+01 | 6.637E-01 | 1.852E+02 | 1.244E-02 |
| 2070 | 1.494E+03 | 8.161E+05 | 5.483E+01 | 6.377E-01 | 1.779E+02 | 1.195E-02 |
| 2071 | 1.435E+03 | 7.841E+05 | 5.268E+01 | 6.127E-01 | 1.709E+02 | 1.149E-02 |
| 2072 | 1.379E+03 | 7.534E+05 | 5.062E+01 | 5.887E-01 | 1.642E+02 | 1.103E-02 |
| 2073 | 1.325E+03 | 7.238E+05 | 4.863E+01 | 5.656E-01 | 1.578E+02 | 1.060E-02 |
| 2074 | 1.273E+03 | 6.954E+05 | 4.673E+01 | 5.434E-01 | 1.516E+02 | 1.019E-02 |
| 2075 | 1.223E+03 | 6.682E+05 | 4.489E+01 | 5.221E-01 | 1.457E+02 | 9.787E-03 |
| 2076 | 1.175E+03 | 6.420E+05 | 4.313E+01 | 5.016E-01 | 1.399E+02 | 9.403E-03 |
| 2077 | 1.129E+03 | 6.168E+05 | 4.144E+01 | 4.820E-01 | 1.345E+02 | 9.034E-03 |
| 2078 | 1.085E+03 | 5.926E+05 | 3.982E+01 | 4.631E-01 | 1.292E+02 | 8.680E-03 |
| 2079 | 1.042E+03 | 5.694E+05 | 3.826E+01 | 4.449E-01 | 1.241E+02 | 8.340E-03 |
| 2080 | 1.001E+03 | 5.471E+05 | 3.676E+01 | 4.275E-01 | 1.193E+02 | 8.013E-03 |
| 2081 | 9.621E+02 | 5.256E+05 | 3.532E+01 | 4.107E-01 | 1.146E+02 | 7.699E-03 |
| 2082 | 9.244E+02 | 5.050E+05 | 3.393E+01 | 3.946E-01 | 1.101E+02 | 7.397E-03 |
| 2083 | 8.881E+02 | 4.852E+05 | 3.260E+01 | 3.791E-01 | 1.058E+02 | 7.107E-03 |
| 2084 | 8.533E+02 | 4.662E+05 | 3.132E+01 | 3.643E-01 | 1.016E+02 | 6.828E-03 |
| 2085 | 8.199E+02 | 4.479E+05 | 3.009E+01 | 3.500E-01 | 9.764E+01 | 6.560E-03 |
| 2086 | 7.877E+02 | 4.303E+05 | 2.891E+01 | 3.363E-01 | 9.381E+01 | 6.303E-03 |
| 2087 | 7.568E+02 | 4.135E+05 | 2.778E+01 | 3.231E-01 | 9.013E+01 | 6.056E-03 |
| 2088 | 7.271E+02 | 3.972E+05 | 2.669E+01 | 3.104E-01 | 8.660E+01 | 5.819E-03 |
| 2089 | 6.986E+02 | 3.817E+05 | 2.564E+01 | 2.982E-01 | 8.320E+01 | 5.590E-03 |
| 2090 | 6.712E+02 | 3.667E+05 | 2.464E+01 | 2.865E-01 | 7.994E+01 | 5.371E-03 |
| 2091 | 6.449E+02 | 3.523E+05 | 2.367E+01 | 2.753E-01 | 7.681E+01 | 5.161E-03 |
| 2092 | 6.196E+02 | 3.385E+05 | 2.274E+01 | 2.645E-01 | 7.379E+01 | 4.958E-03 |
| 2093 | 5.953E+02 | 3.252E+05 | 2.185E+01 | 2.541E-01 | 7.090E+01 | 4.764E-03 |
| 2094 | 5.720E+02 | 3.125E+05 | 2.100E+01 | 2.442E-01 | 6.812E+01 | 4.577E-03 |
| 2095 | 5.496E+02 | 3.002E+05 | 2.017E+01 | 2.346E-01 | 6.545E+01 | 4.398E-03 |
| 2096 | 5.280E+02 | 2.885E+05 | 1.938E+01 | 2.254E-01 | 6.288E+01 | 4.225E-03 |
| 2097 | 5.073E+02 | 2.771E+05 | 1.862E+01 | 2.166E-01 | 6.042E+01 | 4.059E-03 |
| 2098 | 4.874E+02 | 2.663E+05 | 1.789E+01 | 2.081E-01 | 5.805E+01 | 3.900E-03 |
| 2099 | 4.683E+02 | 2.558E+05 | 1.719E+01 | 1.999E-01 | 5.577E+01 | 3.747E-03 |
| 2100 | 4.499E+02 | 2.458E+05 | 1.652E+01 | 1.921E-01 | 5.359E+01 | 3.600E-03 |

Results (Continued)

| Year | Carbon dioxide | | | NMOC | | |
|------|----------------|------------------------|---------------------------|-----------|------------------------|---------------------------|
| | (Mg/year) | (m ³ /year) | (av ft ³ /min) | (Mg/year) | (m ³ /year) | (av ft ³ /min) |
| 2101 | 4.323E+02 | 2.362E+05 | 1.587E+01 | 1.845E-01 | 5.148E+01 | 3.459E-03 |
| 2102 | 4.154E+02 | 2.269E+05 | 1.525E+01 | 1.773E-01 | 4.947E+01 | 3.324E-03 |
| 2103 | 3.991E+02 | 2.180E+05 | 1.465E+01 | 1.704E-01 | 4.753E+01 | 3.193E-03 |
| 2104 | 3.834E+02 | 2.095E+05 | 1.407E+01 | 1.637E-01 | 4.566E+01 | 3.068E-03 |
| 2105 | 3.684E+02 | 2.012E+05 | 1.352E+01 | 1.573E-01 | 4.387E+01 | 2.948E-03 |
| 2106 | 3.539E+02 | 1.934E+05 | 1.299E+01 | 1.511E-01 | 4.215E+01 | 2.832E-03 |
| 2107 | 3.401E+02 | 1.858E+05 | 1.248E+01 | 1.452E-01 | 4.050E+01 | 2.721E-03 |
| 2108 | 3.267E+02 | 1.785E+05 | 1.199E+01 | 1.395E-01 | 3.891E+01 | 2.614E-03 |
| 2109 | 3.139E+02 | 1.715E+05 | 1.152E+01 | 1.340E-01 | 3.739E+01 | 2.512E-03 |
| 2110 | 3.016E+02 | 1.648E+05 | 1.107E+01 | 1.288E-01 | 3.592E+01 | 2.413E-03 |
| 2111 | 2.898E+02 | 1.583E+05 | 1.064E+01 | 1.237E-01 | 3.451E+01 | 2.319E-03 |
| 2112 | 2.784E+02 | 1.521E+05 | 1.022E+01 | 1.189E-01 | 3.316E+01 | 2.228E-03 |
| 2113 | 2.675E+02 | 1.461E+05 | 9.819E+00 | 1.142E-01 | 3.186E+01 | 2.141E-03 |
| 2114 | 2.570E+02 | 1.404E+05 | 9.434E+00 | 1.097E-01 | 3.061E+01 | 2.057E-03 |
| 2115 | 2.469E+02 | 1.349E+05 | 9.064E+00 | 1.054E-01 | 2.941E+01 | 1.976E-03 |
| 2116 | 2.373E+02 | 1.296E+05 | 8.709E+00 | 1.013E-01 | 2.826E+01 | 1.898E-03 |
| 2117 | 2.280E+02 | 1.245E+05 | 8.367E+00 | 9.731E-02 | 2.715E+01 | 1.824E-03 |
| 2118 | 2.190E+02 | 1.196E+05 | 8.039E+00 | 9.349E-02 | 2.608E+01 | 1.753E-03 |
| 2119 | 2.104E+02 | 1.150E+05 | 7.724E+00 | 8.983E-02 | 2.506E+01 | 1.684E-03 |
| 2120 | 2.022E+02 | 1.104E+05 | 7.421E+00 | 8.631E-02 | 2.408E+01 | 1.618E-03 |
| 2121 | 1.942E+02 | 1.061E+05 | 7.130E+00 | 8.292E-02 | 2.313E+01 | 1.554E-03 |
| 2122 | 1.866E+02 | 1.020E+05 | 6.850E+00 | 7.967E-02 | 2.223E+01 | 1.493E-03 |
| 2123 | 1.793E+02 | 9.796E+04 | 6.582E+00 | 7.655E-02 | 2.135E+01 | 1.435E-03 |
| 2124 | 1.723E+02 | 9.412E+04 | 6.324E+00 | 7.354E-02 | 2.052E+01 | 1.379E-03 |
| 2125 | 1.655E+02 | 9.043E+04 | 6.076E+00 | 7.066E-02 | 1.971E+01 | 1.325E-03 |
| 2126 | 1.590E+02 | 8.688E+04 | 5.838E+00 | 6.789E-02 | 1.894E+01 | 1.273E-03 |
| 2127 | 1.528E+02 | 8.347E+04 | 5.609E+00 | 6.523E-02 | 1.820E+01 | 1.223E-03 |
| 2128 | 1.468E+02 | 8.020E+04 | 5.389E+00 | 6.267E-02 | 1.748E+01 | 1.175E-03 |
| 2129 | 1.411E+02 | 7.706E+04 | 5.177E+00 | 6.021E-02 | 1.680E+01 | 1.129E-03 |
| 2130 | 1.355E+02 | 7.404E+04 | 4.974E+00 | 5.785E-02 | 1.614E+01 | 1.084E-03 |
| 2131 | 1.302E+02 | 7.113E+04 | 4.779E+00 | 5.558E-02 | 1.551E+01 | 1.042E-03 |
| 2132 | 1.251E+02 | 6.834E+04 | 4.592E+00 | 5.340E-02 | 1.490E+01 | 1.001E-03 |
| 2133 | 1.202E+02 | 6.566E+04 | 4.412E+00 | 5.131E-02 | 1.431E+01 | 9.618E-04 |
| 2134 | 1.155E+02 | 6.309E+04 | 4.239E+00 | 4.930E-02 | 1.375E+01 | 9.241E-04 |
| 2135 | 1.110E+02 | 6.062E+04 | 4.073E+00 | 4.737E-02 | 1.321E+01 | 8.879E-04 |
| 2136 | 1.066E+02 | 5.824E+04 | 3.913E+00 | 4.551E-02 | 1.270E+01 | 8.530E-04 |
| 2137 | 1.024E+02 | 5.595E+04 | 3.760E+00 | 4.372E-02 | 1.220E+01 | 8.196E-04 |
| 2138 | 9.841E+01 | 5.376E+04 | 3.612E+00 | 4.201E-02 | 1.172E+01 | 7.875E-04 |
| 2139 | 9.455E+01 | 5.165E+04 | 3.471E+00 | 4.036E-02 | 1.126E+01 | 7.566E-04 |
| 2140 | 9.084E+01 | 4.963E+04 | 3.334E+00 | 3.878E-02 | 1.082E+01 | 7.269E-04 |

Stage I
Cells 1 through Cell 4
Mueller Equation Calculations

JOB Forty West Landfill, Cells 1-4
DESCRIPTION Mueller Equation Calcs

PROJECT NO. 13813514.00001
COMPUTED BY KMC
CHECKED BY NSG/JDM

DATE: 01 Dec 2009
DATE: 18 Jan 2010

Calculation Methodology Stage 1 - Cells 1 through 4

I. OBJECTIVE

To prepare a detailed design of an active gas collection system for use by Washington Renewable Energy to construct the system in existing Cells 1, 2, 3, and 4. The attached calculations performed are to properly size the header piping system based on the information provided.

II. ASSUMPTIONS

- 1 Landfill gas production is based on the LandGEM model provided by U.S. EPA. The following assumptions were used for the LandGEM model:
 - a: Methane Generation Rate, $k = 0.04$ (Inventory Conventional)
 - b: Potential Methane Generation Capacity, $L_0 = 100$ (Inventory Conventional)
 - c: NMOC Concentration, 109 ppmv as hexane (based on Tier 2 Landfill Gas Analysis Report performed by URS submitted July 17, 2007).
 - d: Methane Content, 50% by volume (CAA)
 - e: 1% annual growth on waste placement on years after 2009.
- 2 Landfill Design Capacity for Cells 1 through 4 is 2,428,200 short tons. This value was obtained from most recent aerial photogrammetry data provided by Aerometric, Inc. for Cells 1 through 3 (1,859,000 yd³) and design values for Cell 4 (2,188,000 yd³). The sum of volume available is then multiplied by the average density of the waste received by the facility (0.60 tons/yd³).
- 3 The system pressure of the header system is assumed to be 2.0 psia and the specific density of the landfill gas is similar to that of air (1.0). These values are typical for MSW landfills.
- 4 The temperature of the gas within the header system is assumed to be 100°F and fully saturated. This value is a conservative value for MSW landfills.

III. CALCULATIONS AND PROCEDURES

- 1 The Radius of Influence (ROI) is the effective area around the vertical gas extraction well applied by the vacuum. The ROI is obtained using the EPA Method with the following equation:

$$R = 1311 \times \left[\frac{QDC}{LQ_{well}} \right]^{1/2}$$

The equation is based on the number of wells in operation within the system and the gas generated by the system. Using the maximum values generated by LandGEM and typical values found in MSW landfills, the ROI typically ranges around 200 feet. In order to be conservative, a spacing of 175 feet was used to accomplish overlap in coverage.

- 2 Using a 175 feet offset for each vertical well, a total of 55 extraction wells were required for Cells 1 through 4. The individual wells were then connected to a proposed header located outside the limits of waste through a total of 19 laterals.
- 3 The maximum flow of gas handled by the extraction system is based on the LandGEM model. The maximum flow is then divided by the footprint of the cells to get an expected flow per square feet. The flow per square foot was found to be approximately 3.795×10^{-4} ft³/min.
- 4 To determine the maximum flow for each lateral, the total number of wells within the cells is divided into the footprint for each cell. The flow is then multiplied by the number of wells connected to each lateral (node) at the the connection to the header pipe.
- 5 The Low Pressure Mueller Equation is then used to determine the pressure the system must overcome in the design and selection of a blower. Using an iterative process, the pipe diameter of header is determined by minimizing the head required of the blower.

$$\Delta p = L \left(\frac{60 \times Q \times G^{0.425}}{2971 \times d^{2.725}} \right)^{0.575} = \left[\frac{Q}{49.52 \times d^{2.725}} \right]^{0.575}$$

The flow, "Q" is solved for above, "d" is equal to the pipe diameter, and "G" is assumed to be 1 for the specific density of the gas.

- 6 The velocity of the gas is then determined using the continuity equation.

$$Q = AV$$

JOB Forty West Landfill - Cells 1 - 4

PROJECT NO.: 13813514.00001

DATE: 29-Jan-10

DESCRIPTION Mueller Equation Calculation Summary

COMPUTED BY KMC

DATE: 29-Jan-10

CHECKED BY NSG/JDM

DATE: 1-Feb-10

| | Total Flow (scfm) | Headloss (in H ₂ O) |
|----------------------|-------------------|--------------------------------|
| South Header | 843.41 | 9.29 |
| Flare Station Piping | 1728.69 | 0.17 |

Total Headloss (max.)

9.47

Operational Head

10.00

Total Vacuum Required

19.47

- 1) Operational head is the theoretical vacuum available at the most remote wellhead.
- 2) System minor losses are accounted for by the pressure drop safety factor of 1.5.

JOB DESCRIPTION Forty West Landfill, Cells 1-4 Header
Mueller Equation Calcs.

PROJECT NO.: 138T3514.00001
 COMPUTED BY KMC
 CHECKED BY NSG/JDM

DATE: 1-Dec-09
 DATE: 18-Jan-10

| Primary Header Pipe in Cells I-IV | |
|---|-----------------------|
| Total Header Pipe Length (Slope Adjusted) | 14,582.59 lineal feet |
| Node Separation CFM/Node | 263.27 feet (max) |
| Allowable Pressure Drop | varies |
| Pressure Drop Safety Factor | 1.50 |
| Pipe Diameter | 12.00 inches |
| Cumulative Pressure Drop | 843.41 scfm |
| Accumulated Flow | 843.41 scfm |

Effective Area 51.02 acres
 Total Gas Generation 843.41 scfm
 Flow/ft² 0.0003795 cfm/ft²

Gas from S Header 843.41 scfm
 Total Gas Collected 843.41 scfm

| Cell 4 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-------------------------|---------------------------|-----------|--------------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in) | Slope (%) | Gas Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | 617,245.20 | | | | | | | | | | | |
| HW-4-1 | 1 | 123,449.04 | 46.85 | 646.47 | 46.85 | 2.82 | 6 | 0.000280 | 0.180799 | 3.00 | 1.66 | 0.12 | 0.06 |
| 4A | 0 | - | - | 635.50 | 46.85 | 2.82 | 12 | 0.000010 | 0.006653 | 2.00 | 0.41 | 0.12 | 0.08 |
| 4B | 1 | 123,449.04 | 46.85 | 697.26 | 93.70 | 3.64 | 12 | 0.000035 | 0.024369 | 2.00 | 0.83 | 0.25 | 0.08 |
| 4C | 1 | 123,449.04 | 46.85 | 790.92 | 140.55 | 4.22 | 12 | 0.000071 | 0.055953 | 2.00 | 1.24 | 0.37 | 0.10 |
| 4D | 1 | 123,449.04 | 46.85 | 697.33 | 187.40 | 4.69 | 12 | 0.000117 | 0.081361 | 2.00 | 1.66 | 0.49 | 0.12 |
| 4E | 1 | 123,449.04 | 46.85 | 836.66 | 234.24 | 5.09 | 12 | 0.000172 | 0.143902 | 2.00 | 2.07 | 0.62 | 0.13 |
| Totals | 5 | 493,796.16 | | 3,657.67 | | | | | 0.312239 | | | | |

| Cell 3 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-------------------------|---------------------------|-----------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in) | Slope (%) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | 634,233.60 | | | | | | | | | | | |
| 3A | 3 | 90,604.80 | 34.38 | 740.41 | 268.63 | 5.35 | 12 | 0.000218 | 0.161599 | 2.00 | 2.38 | 0.71 | 0.14 |
| 3B | 4 | 120,806.40 | 45.85 | 686.75 | 314.48 | 5.67 | 12 | 0.000287 | 0.197143 | 2.00 | 2.78 | 0.83 | 0.15 |
| 3C | 3 | 90,604.80 | 34.38 | 647.40 | 348.86 | 5.89 | 12 | 0.000344 | 0.222601 | 2.00 | 3.08 | 0.92 | 0.16 |
| 3D | 4 | 120,806.40 | 45.85 | 694.56 | 394.71 | 6.17 | 12 | 0.000426 | 0.296020 | 2.00 | 3.49 | 1.04 | 0.16 |
| 3E | 3 | 90,604.80 | 34.38 | 647.88 | 429.09 | 6.36 | 12 | 0.000493 | 0.319296 | 2.00 | 3.79 | 1.13 | 0.17 |
| 3F | 4 | 120,806.40 | 45.85 | 609.78 | 474.94 | 6.60 | 12 | 0.000588 | 0.358546 | 2.00 | 4.20 | 1.25 | 0.17 |
| Totals | 21 | 634,233.60 | | 4,026.78 | | | | | 1.555204 | | | | |

| Cell 2 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-------------------------|---------------------------|-----------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in) | Slope (%) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | 470,448.00 | | | | | | | | | | | |
| 2A | 3 | 88,209.00 | 33.48 | 723.34 | 508.41 | 6.77 | 12 | 0.000662 | 0.478804 | 2.00 | 4.50 | 1.34 | 0.18 |
| 2B | 4 | 117,612.00 | 44.63 | 675.28 | 553.05 | 6.98 | 12 | 0.000766 | 0.517435 | 2.00 | 4.89 | 1.46 | 0.19 |
| 2C | 2 | 59,806.00 | 22.32 | 780.61 | 575.36 | 7.08 | 12 | 0.000821 | 0.640745 | 2.00 | 5.09 | 1.52 | 0.19 |
| 2D | 3 | 88,209.00 | 33.48 | 904.17 | 608.84 | 7.23 | 12 | 0.000905 | 0.818869 | 2.00 | 5.38 | 1.61 | 0.20 |
| 2E | 4 | 117,612.00 | 44.63 | 991.07 | 653.47 | 7.42 | 12 | 0.001024 | 1.015088 | 2.00 | 5.78 | 1.73 | 0.20 |
| Totals | 16 | 470,448.00 | | 4,074.47 | | | | | 3.470941 | | | | |

| Cell 1 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-------------------------|---------------------------|-----------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in) | Slope (%) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | 500,504.40 | | | | | | | | | | | |
| 1A | 5 | 192,501.69 | 73.05 | 1157.17 | 726.53 | 7.71 | 12 | 0.001231 | 1.425080 | 2.00 | 6.42 | 1.92 | 0.21 |
| 1B | 5 | 192,501.69 | 73.05 | 878.2 | 799.58 | 7.99 | 12 | 0.001455 | 1.277622 | 2.00 | 7.07 | 2.11 | 0.22 |
| 1C | 3 | 115,501.02 | 43.83 | 785.38 | 843.41 | 8.15 | 12 | 0.001596 | 1.253714 | 2.00 | 7.46 | 2.23 | 0.23 |
| Totals | 13 | 500,504.40 | | 2,820.75 | | | | | 3.956416 | | | | |

| | | | | | | | | | | | | | |
|--------------------|----|--------------|--|-----------|--------|--|--|--|------|--|--|--|--|
| Cumulative Totals: | 55 | 2,098,982.16 | | 14,579.67 | 843.41 | | | | 9.29 | | | | |
|--------------------|----|--------------|--|-----------|--------|--|--|--|------|--|--|--|--|

JOB DESCRIPTION Forty West Landfill, Cells 1 - 4
Mueller Equation Calcs. (PIPE TO FLARE STATION)

PROJECT NO.: 13813514.00001
 COMPUTED BY: KMC
 CHECKED BY: NSG/JDM

DATE: 29-Jan-10
 DATE: _____

The worst case lateral calculation is intended to ensure that the dimensions specified for the entire system is properly sized to accommodate the losses from the farthest well from the blower.

SUMMARY OF RESULTS FOR PIPE TO FLARE STATION

| | |
|-----------------------------|------|
| Allowable Pressure Drop | 0.01 |
| Pressure Drop Safety Factor | 1.50 |

Total Landfill Area* 188.99 acres 8,232,404.40 ft²
 Total Gas Generation 843.41 scfm**
 Flow/ft² 0.00010245 cfm/ft²

Gas from N Header - scfm
 Gas from S Header 843.41 scfm
 Total Gas Collected 843.41 scfm

| Pipe to Flare Station | | | | | | | | | | | | | |
|-----------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-----------------------------|--|-----------|--------------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Max Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) | Gas Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| Pipe to Flare | n/a | n/a | n/a | 311.12 | 843.41 | 8.15 | 15 | 0.000554 | 0.172771 | 6.00 | 4.77 | 2.23 | |

Closure
Cells 1 through Cells 14
LandGEM Calculations

JOB Forty West Landfill, Phase 1 - 2
DESCRIPTION Mueller Equation Calcs

PROJECT NO. 13813514.00001
COMPUTED BY KMC
CHECKED BY NSG/JDM

DATE: 01 Dec 2009
DATE: 18 Jan 2010

Calculation Methodology - At Closure

I. OBJECTIVE

To prepare a detailed design of an active gas collection system for use by Washington Renewable Energy to construct the system through Phase 1 and Phase 2 of the Forty West Landfill in Hagerstown, Maryland. The attached calculations performed are to provide a preliminary size the header piping system based on the preliminary layout for Stage 2 (Cells 5, 6, and 7) and a preliminary layout of Phase 2 (Cells 8 through 14). Design calculations should be revised based on the future LFG system layout.

II. ASSUMPTIONS

- 1 Landfill gas production is based on the LandGEM model provided by U.S. EPA. The following assumptions were used for the LandGEM model:
 - a: Methane Generation Rate, $k = 0.04$ (Inventory Conventional)
 - b: Potential Methane Generation Capacity, $L_0 = 100$ (Inventory Conventional)
 - c: NMOC Concentration, 109 ppmv as hexane (based on Tier 2 Landfill Gas Analysis Report performed by URS submitted July 17, 2007).
 - d: Methane Content, 50% by volume (CAA)
 - e: 1% annual growth on waste placement on years after 2009.
- 2 Landfill Design Capacity for the landfill is 7,402,496 short tons. This value is based from most recent aerial photogrammetry data provided by Aerometric, Inc. for Cells 1 through 3 (1,859,000 yd³) and design values for Cells 4 through 14 (10,478,493 yd³). The sum of volume available is then multiplied by the average density of the waste received by the facility (0.60 tons/yd³).
- 3 The system pressure (vacuum) of the header system is assumed to be 2.0 psia and the specific density of the landfill gas is similar to that of air (1.0). These values are typical for MSW landfills and landfill gas collection systems (taken from *Landfill Gas System Engineering Design Courseware by Landtec Corp.*).
- 4 The temperature of the gas within the header system is assumed to be 100°F and fully saturated. This value is a conservative value for MSW landfills.

III. CALCULATIONS AND PROCEDURES

- 1 The Radius of Influence (ROI) is the effective area around the vertical gas extraction well applied by the vacuum. The ROI is obtained using the EPA Method with the following equation:

$$R = 1311 \times \left[\frac{QDC}{LQ_{well}} \right]^{1/2}$$

The equation is based on the number of wells in operation within the system and the gas generated by the system. Using the maximum values generated by LandGEM and typical values found in MSW landfills, the ROI typically ranges around 200 feet. In order to be conservative, a spacing of 175 feet was used to accomplish overlap in coverage.

- 2 Using a 175 feet offset for each vertical well, a total of 35 extraction wells were required for the northern section of the system (Northern Header) and 84 extraction wells for the southern section of the system (Southern Header). The individual wells were then connected to a proposed header located outside the limits of waste through a total of 63 laterals and 119 extraction wells for the entire site at final completion.
- 3 The maximum flow of gas handled by the extraction system is based on the LandGEM model. The maximum flow is then divided by the footprint of the cells to get an expected flow per square feet. The flow per square feet was found to be approximately 2.8×10^{-4} ft³/min.
- 4 To determine the maximum flow for each lateral, the effective area for each cell is divided into the total number of wells within the cells. The flow is then multiplied by the number of wells connected to each lateral (node) at the connection to the header pipe.
- 5 The Low Pressure Mueller Equation is then used to determine the pressure the system must overcome in the design and selection of a blower. Using an iterative process, the pipe diameter of header is determined by minimizing the head required of the blower.

$$\Delta p = L \left(\frac{60 \times Q \times G^{0.425}}{2971 \times d^{2.725}} \right)^{0.575} = \left[\frac{Q}{49.52 \times d^{2.725}} \right]^{0.575}$$

JOB Forty West Landfill, Phase 1 - 2
DESCRIPTION Mueller Equation Calcs

PROJECT NO. 13813514.00001
COMPUTED BY KMC
CHECKED BY NSG/JDM

DATE: 01 Dec 2009
DATE: 18 Jan 2010

The flow, "Q" is solved for above, "d" is equal to the pipe diameter, and "G" is assumed to be 1 for the specific density of the gas.

6 The velocity of the gas is then determined using the continuity equation.

$$Q = AV$$

7 The accumulated condensate production is calculated by using Antoine's Equation.

$$V_{(cond)} = \frac{5,694 \times 10^{\beta}}{P_s}$$

$$\beta = 6.32 - \frac{3,081}{T + 385}$$

The volume produced per million cubic foot of LFG calculated by Antoine's Equation is then multiplied by the flow of LFG to find the rate of condensate produced. Where P_s = system pressure in psia and T = temperature of the landfill gas within the header system in °F.

8 Using Manning's Formula for gravity flow, solve for the depth of the condensate based on the pipe's slope, pipe size, and flow.

IV. RESULTS

The active gas extraction system will require a blower capable of producing a vacuum at 48.12" H₂O at a flow rate of a 1,728 scfm at landfill closure. The system is divided into two sections, a north header and a south header. The North Header was found to require a flowrate of 970 scfm of gas at a vacuum of 28.11 inches of water while the south requires flowrate of approximately 758 scfm at a vacuum of 32.5 inches of water.



Summary Report

Landfill Name or Identifier: Forty West Landfill--Phase 1 and Phase 2

Date: Friday, February 19, 2010

Description/Comments:

*Assuming 1% annual waste placement increase after 2008.

**Landfill Design Capacity for the landfill is 7,402,496 short tons. This value is based from data provided by Buchart-horn, Inc. for Cells 1 through 3 (1,859,000 yd³) and design values for Cells 4 through 14 (10,478,493 yd³). The sum of volume available is then multiplied by the average density of the waste received by the facility (0.60 tons/yd³).

About LandGEM:

First-Order Decomposition Rate Equation:

$$Q_{CH_4} = \sum_{i=1}^n \sum_{j=0.1}^1 kL_o \left(\frac{M_i}{10} \right) e^{-kt_{ij}}$$

Where,

Q_{CH_4} = annual methane generation in the year of the calculation ($m^3/year$)

i = 1-year time increment

n = (year of the calculation) - (initial year of waste acceptance)

j = 0.1-year time increment

k = methane generation rate ($year^{-1}$)

L_o = potential methane generation capacity (m^3/Mg)

M_i = mass of waste accepted in the i^{th} year (Mg)

t_{ij} = age of the j^{th} section of waste mass M_i accepted in the i^{th} year
(decimal years, e.g., 3.2 years)

LandGEM is based on a first-order decomposition rate equation for quantifying emissions from the decomposition of landfilled waste in municipal solid waste (MSW) landfills. The software provides a relatively simple approach to estimating landfill gas emissions. Model defaults are based on empirical data from U.S. landfills. Field test data can also be used in place of model defaults when available. Further guidance on EPA test methods, Clean Air Act (CAA) regulations, and other guidance regarding landfill gas emissions and control technology requirements can be found at <http://www.epa.gov/ttnatw01/landfill/landflpg.html>.

LandGEM is considered a screening tool — the better the input data, the better the estimates. Often, there are limitations with the available data regarding waste quantity and composition, variation in design and operating practices over time, and changes occurring over time that impact the emissions potential. Changes to landfill operation, such as operating under wet conditions through leachate recirculation or other liquid additions, will result in generating more gas at a faster rate. Defaults for estimating emissions for this type of operation are being developed to include in LandGEM along with defaults for conventional landfills (no leachate or liquid additions) for developing emission inventories and determining CAA applicability. Refer to the Web site identified above for future updates.

Input Review

LANDFILL CHARACTERISTICS

| | | |
|--|-----------|------------|
| Landfill Open Year | 2000 | |
| Landfill Closure Year (with 80-year limit) | 2047 | |
| Actual Closure Year (without limit) | 2047 | |
| Have Model Calculate Closure Year? | Yes | |
| Waste Design Capacity | 7,402,496 | short tons |

MODEL PARAMETERS

| | | |
|---|-------|--------------------|
| Methane Generation Rate, k | 0.040 | year ⁻¹ |
| Potential Methane Generation Capacity, L ₀ | 100 | m ³ /Mg |
| NMOC Concentration | 109 | ppmv as hexane |
| Methane Content | 50 | % by volume |

GASES / POLLUTANTS SELECTED

| | |
|---------------------|--------------------|
| Gas / Pollutant #1: | Total landfill gas |
| Gas / Pollutant #2: | Methane |
| Gas / Pollutant #3: | Carbon dioxide |
| Gas / Pollutant #4: | NMOC |

WASTE ACCEPTANCE RATES

| Year | Waste Accepted | | Waste-In-Place | |
|------|----------------|-------------------|----------------|--------------|
| | (Mg/year) | (short tons/year) | (Mg) | (short tons) |
| 2000 | 1,818 | 2,000 | 0 | 0 |
| 2001 | 92,454 | 101,699 | 1,818 | 2,000 |
| 2002 | 108,285 | 119,113 | 94,272 | 103,699 |
| 2003 | 119,441 | 131,385 | 202,556 | 222,812 |
| 2004 | 136,451 | 150,096 | 321,997 | 354,197 |
| 2005 | 158,062 | 173,868 | 458,448 | 504,293 |
| 2006 | 141,335 | 155,468 | 616,510 | 678,161 |
| 2007 | 121,698 | 133,868 | 757,845 | 833,629 |
| 2008 | 120,305 | 132,336 | 879,543 | 967,497 |
| 2009 | 121,509 | 133,659 | 999,848 | 1,099,833 |
| 2010 | 122,724 | 134,996 | 1,121,357 | 1,233,492 |
| 2011 | 123,951 | 136,346 | 1,244,080 | 1,368,488 |
| 2012 | 125,190 | 137,709 | 1,368,031 | 1,504,834 |
| 2013 | 126,442 | 139,086 | 1,493,221 | 1,642,544 |
| 2014 | 127,707 | 140,477 | 1,619,664 | 1,781,630 |
| 2015 | 128,984 | 141,882 | 1,747,370 | 1,922,107 |
| 2016 | 130,274 | 143,301 | 1,876,354 | 2,063,989 |
| 2017 | 131,576 | 144,734 | 2,006,628 | 2,207,290 |
| 2018 | 132,892 | 146,181 | 2,138,204 | 2,352,024 |
| 2019 | 134,221 | 147,643 | 2,271,096 | 2,498,206 |
| 2020 | 135,563 | 149,120 | 2,405,317 | 2,645,849 |
| 2021 | 136,919 | 150,611 | 2,540,880 | 2,794,968 |
| 2022 | 138,288 | 152,117 | 2,677,799 | 2,945,579 |
| 2023 | 139,671 | 153,638 | 2,816,087 | 3,097,696 |
| 2024 | 141,068 | 155,174 | 2,955,758 | 3,251,334 |
| 2025 | 142,478 | 156,726 | 3,096,826 | 3,406,508 |
| 2026 | 143,903 | 158,293 | 3,239,304 | 3,563,234 |
| 2027 | 145,342 | 159,876 | 3,383,207 | 3,721,528 |
| 2028 | 146,796 | 161,475 | 3,528,549 | 3,881,404 |
| 2029 | 148,263 | 163,090 | 3,675,345 | 4,042,879 |
| 2030 | 149,746 | 164,721 | 3,823,608 | 4,205,969 |
| 2031 | 151,244 | 166,368 | 3,973,354 | 4,370,690 |
| 2032 | 152,756 | 168,032 | 4,124,598 | 4,537,057 |
| 2033 | 154,284 | 169,712 | 4,277,354 | 4,705,089 |
| 2034 | 155,826 | 171,409 | 4,431,637 | 4,874,801 |
| 2035 | 157,385 | 173,123 | 4,587,464 | 5,046,210 |
| 2036 | 158,959 | 174,854 | 4,744,848 | 5,219,333 |
| 2037 | 160,548 | 176,603 | 4,903,807 | 5,394,188 |
| 2038 | 162,154 | 178,369 | 5,064,355 | 5,570,790 |
| 2039 | 163,775 | 180,153 | 5,226,508 | 5,749,159 |

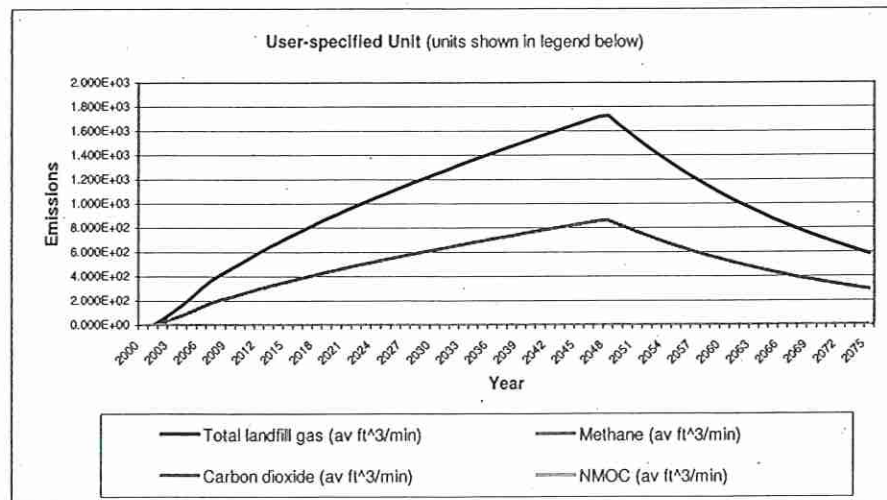
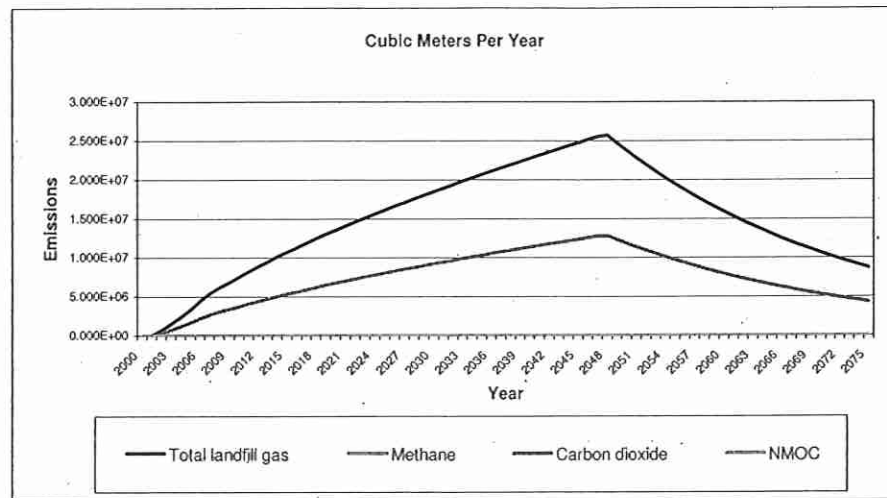
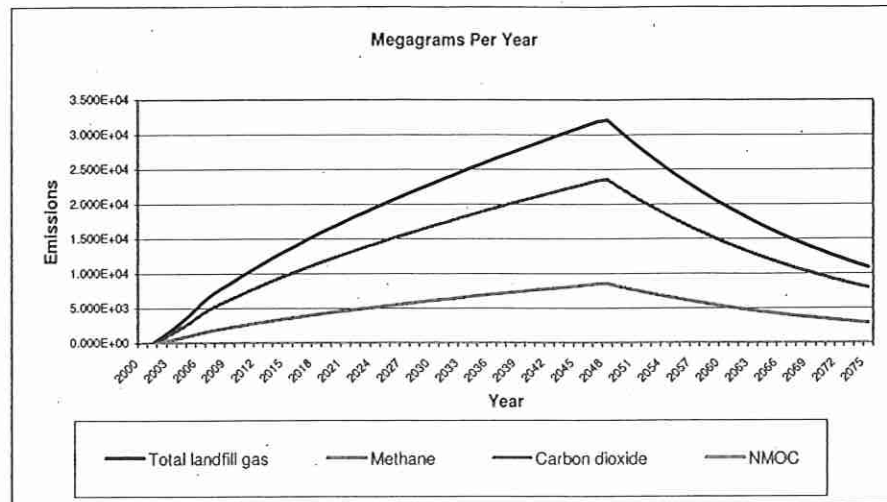
WASTE ACCEPTANCE RATES (Continued)

| Year | Waste Accepted | | Waste-In-Place | |
|------|----------------|-------------------|----------------|--------------|
| | (Mg/year) | (short tons/year) | (Mg) | (short tons) |
| 2040 | 165,413 | 181,954 | 5,390,284 | 5,929,312 |
| 2041 | 167,067 | 183,774 | 5,555,696 | 6,111,266 |
| 2042 | 168,738 | 185,611 | 5,722,763 | 6,295,040 |
| 2043 | 170,425 | 187,468 | 5,891,501 | 6,480,651 |
| 2044 | 172,129 | 189,342 | 6,061,926 | 6,668,119 |
| 2045 | 173,851 | 191,236 | 6,234,055 | 6,857,461 |
| 2046 | 175,589 | 193,148 | 6,407,906 | 7,048,697 |
| 2047 | 146,047 | 160,651 | 6,583,495 | 7,241,845 |
| 2048 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2049 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2050 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2051 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2052 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2053 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2054 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2055 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2056 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2057 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2058 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2059 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2060 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2061 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2062 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2063 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2064 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2065 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2066 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2067 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2068 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2069 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2070 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2071 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2072 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2073 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2074 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2075 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2076 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2077 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2078 | 0 | 0 | 6,729,542 | 7,402,496 |
| 2079 | 0 | 0 | 6,729,542 | 7,402,496 |

Pollutant Parameters

| Gas / Pollutant Default Parameters: | | | | User-specified Pollutant Parameters: | |
|-------------------------------------|--|----------------------|------------------|--------------------------------------|------------------|
| | Compound | Concentration (ppmv) | Molecular Weight | Concentration (ppmv) | Molecular Weight |
| Gases | Total landfill gas | | 0.00 | | |
| | Methane | | 16.04 | | |
| | Carbon dioxide | | 44.01 | | |
| | NMOC | 4,000 | 86.18 | | |
| Pollutants | 1,1,1-Trichloroethane (methyl chloroform) - HAP | 0.48 | 133.41 | | |
| | 1,1,2,2-Tetrachloroethane - HAP/VOC | 1.1 | 167.85 | | |
| | 1,1-Dichloroethane (ethylidene dichloride) - HAP/VOC | 2.4 | 98.97 | | |
| | 1,1-Dichloroethene (vinylidene chloride) - HAP/VOC | 0.20 | 96.94 | | |
| | 1,2-Dichloroethane (ethylene dichloride) - HAP/VOC | 0.41 | 98.96 | | |
| | 1,2-Dichloropropane (propylene dichloride) - HAP/VOC | 0.18 | 112.99 | | |
| | 2-Propanol (isopropyl alcohol) - VOC | 50 | 60.11 | | |
| | Acetone | 7.0 | 58.08 | | |
| | Acrylonitrile - HAP/VOC | 6.3 | 53.06 | | |
| | Benzene - No or Unknown Co-disposal - HAP/VOC | 1.9 | 78.11 | | |
| | Benzene - Co-disposal - HAP/VOC | 11 | 78.11 | | |
| | Bromodichloromethane - VOC | 3.1 | 163.83 | | |
| | Butane - VOC | 5.0 | 58.12 | | |
| | Carbon disulfide - HAP/VOC | 0.58 | 76.13 | | |
| | Carbon monoxide | 140 | 28.01 | | |
| | Carbon tetrachloride - HAP/VOC | 4.0E-03 | 153.84 | | |
| | Carbonyl sulfide - HAP/VOC | 0.49 | 60.07 | | |
| | Chlorobenzene - HAP/VOC | 0.25 | 112.56 | | |
| | Chlorodifluoromethane | 1.3 | 86.47 | | |
| | Chloroethane (ethyl chloride) - HAP/VOC | 1.3 | 64.52 | | |
| | Chloroform - HAP/VOC | 0.03 | 119.39 | | |
| | Chloromethane - VOC | 1.2 | 50.49 | | |
| | Dichlorobenzene - (HAP for para isomer/VOC) | 0.21 | 147 | | |
| | Dichlorodifluoromethane | 16 | 120.91 | | |
| | Dichlorofluoromethane - VOC | 2.6 | 102.92 | | |
| | Dichloromethane (methylene chloride) - HAP | 14 | 84.94 | | |
| | Dimethyl sulfide (methyl sulfide) - VOC | 7.8 | 62.13 | | |
| | Ethane | 890 | 30.07 | | |
| | Ethanol - VOC | 27 | 46.08 | | |

Graphs



Results

| Year | Total landfill gas | | | Methane | | |
|------|--------------------|------------------------|---------------------------|-----------|------------------------|---------------------------|
| | (Mg/year) | (m ³ /year) | (av ft ³ /min) | (Mg/year) | (m ³ /year) | (av ft ³ /min) |
| 2000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2001 | 1.784E+01 | 1.429E+04 | 9.599E-01 | 4.766E+00 | 7.143E+03 | 4.800E-01 |
| 2002 | 9.244E+02 | 7.402E+05 | 4.973E+01 | 2.469E+02 | 3.701E+05 | 2.487E+01 |
| 2003 | 1.951E+03 | 1.562E+06 | 1.050E+02 | 5.211E+02 | 7.810E+05 | 5.248E+01 |
| 2004 | 3.046E+03 | 2.439E+06 | 1.639E+02 | 8.137E+02 | 1.220E+06 | 8.195E+01 |
| 2005 | 4.266E+03 | 3.416E+06 | 2.295E+02 | 1.139E+03 | 1.708E+06 | 1.148E+02 |
| 2006 | 5.650E+03 | 4.524E+06 | 3.040E+02 | 1.509E+03 | 2.262E+06 | 1.520E+02 |
| 2007 | 6.815E+03 | 5.457E+06 | 3.667E+02 | 1.820E+03 | 2.729E+06 | 1.833E+02 |
| 2008 | 7.742E+03 | 6.199E+06 | 4.165E+02 | 2.068E+03 | 3.100E+06 | 2.083E+02 |
| 2009 | 8.619E+03 | 6.902E+06 | 4.637E+02 | 2.302E+03 | 3.451E+06 | 2.319E+02 |
| 2010 | 9.473E+03 | 7.586E+06 | 5.097E+02 | 2.530E+03 | 3.793E+06 | 2.548E+02 |
| 2011 | 1.031E+04 | 8.253E+06 | 5.545E+02 | 2.753E+03 | 4.126E+06 | 2.773E+02 |
| 2012 | 1.112E+04 | 8.903E+06 | 5.982E+02 | 2.970E+03 | 4.452E+06 | 2.991E+02 |
| 2013 | 1.191E+04 | 9.538E+06 | 6.408E+02 | 3.182E+03 | 4.769E+06 | 3.204E+02 |
| 2014 | 1.268E+04 | 1.016E+07 | 6.825E+02 | 3.388E+03 | 5.079E+06 | 3.412E+02 |
| 2015 | 1.344E+04 | 1.076E+07 | 7.231E+02 | 3.590E+03 | 5.381E+06 | 3.616E+02 |
| 2016 | 1.418E+04 | 1.135E+07 | 7.629E+02 | 3.787E+03 | 5.677E+06 | 3.814E+02 |
| 2017 | 1.490E+04 | 1.193E+07 | 8.017E+02 | 3.980E+03 | 5.966E+06 | 4.009E+02 |
| 2018 | 1.561E+04 | 1.250E+07 | 8.398E+02 | 4.169E+03 | 6.249E+06 | 4.199E+02 |
| 2019 | 1.630E+04 | 1.305E+07 | 8.770E+02 | 4.354E+03 | 6.526E+06 | 4.385E+02 |
| 2020 | 1.698E+04 | 1.360E+07 | 9.135E+02 | 4.535E+03 | 6.798E+06 | 4.567E+02 |
| 2021 | 1.764E+04 | 1.413E+07 | 9.492E+02 | 4.713E+03 | 7.064E+06 | 4.746E+02 |
| 2022 | 1.829E+04 | 1.465E+07 | 9.843E+02 | 4.887E+03 | 7.325E+06 | 4.922E+02 |
| 2023 | 1.893E+04 | 1.516E+07 | 1.019E+03 | 5.058E+03 | 7.581E+06 | 5.094E+02 |
| 2024 | 1.956E+04 | 1.566E+07 | 1.053E+03 | 5.225E+03 | 7.832E+06 | 5.263E+02 |
| 2025 | 2.018E+04 | 1.616E+07 | 1.086E+03 | 5.390E+03 | 8.080E+06 | 5.429E+02 |
| 2026 | 2.079E+04 | 1.665E+07 | 1.118E+03 | 5.552E+03 | 8.323E+06 | 5.592E+02 |
| 2027 | 2.138E+04 | 1.712E+07 | 1.151E+03 | 5.712E+03 | 8.562E+06 | 5.753E+02 |
| 2028 | 2.197E+04 | 1.759E+07 | 1.182E+03 | 5.869E+03 | 8.797E+06 | 5.911E+02 |
| 2029 | 2.255E+04 | 1.806E+07 | 1.213E+03 | 6.024E+03 | 9.029E+06 | 6.066E+02 |
| 2030 | 2.312E+04 | 1.851E+07 | 1.244E+03 | 6.176E+03 | 9.257E+06 | 6.220E+02 |
| 2031 | 2.368E+04 | 1.897E+07 | 1.274E+03 | 6.326E+03 | 9.483E+06 | 6.371E+02 |
| 2032 | 2.424E+04 | 1.941E+07 | 1.304E+03 | 6.475E+03 | 9.705E+06 | 6.521E+02 |
| 2033 | 2.479E+04 | 1.985E+07 | 1.334E+03 | 6.621E+03 | 9.925E+06 | 6.668E+02 |
| 2034 | 2.533E+04 | 2.028E+07 | 1.363E+03 | 6.766E+03 | 1.014E+07 | 6.814E+02 |
| 2035 | 2.587E+04 | 2.071E+07 | 1.392E+03 | 6.909E+03 | 1.036E+07 | 6.958E+02 |
| 2036 | 2.640E+04 | 2.114E+07 | 1.420E+03 | 7.051E+03 | 1.057E+07 | 7.101E+02 |
| 2037 | 2.692E+04 | 2.156E+07 | 1.448E+03 | 7.191E+03 | 1.078E+07 | 7.242E+02 |
| 2038 | 2.744E+04 | 2.197E+07 | 1.476E+03 | 7.330E+03 | 1.099E+07 | 7.382E+02 |
| 2039 | 2.796E+04 | 2.239E+07 | 1.504E+03 | 7.467E+03 | 1.119E+07 | 7.521E+02 |
| 2040 | 2.847E+04 | 2.280E+07 | 1.532E+03 | 7.604E+03 | 1.140E+07 | 7.658E+02 |
| 2041 | 2.897E+04 | 2.320E+07 | 1.559E+03 | 7.739E+03 | 1.160E+07 | 7.794E+02 |
| 2042 | 2.948E+04 | 2.360E+07 | 1.586E+03 | 7.874E+03 | 1.180E+07 | 7.930E+02 |
| 2043 | 2.998E+04 | 2.400E+07 | 1.613E+03 | 8.007E+03 | 1.200E+07 | 8.064E+02 |
| 2044 | 3.047E+04 | 2.440E+07 | 1.640E+03 | 8.140E+03 | 1.220E+07 | 8.198E+02 |
| 2045 | 3.097E+04 | 2.480E+07 | 1.666E+03 | 8.272E+03 | 1.240E+07 | 8.331E+02 |
| 2046 | 3.146E+04 | 2.519E+07 | 1.693E+03 | 8.403E+03 | 1.260E+07 | 8.463E+02 |
| 2047 | 3.195E+04 | 2.558E+07 | 1.719E+03 | 8.534E+03 | 1.279E+07 | 8.595E+02 |
| 2048 | 3.213E+04 | 2.573E+07 | 1.729E+03 | 8.582E+03 | 1.286E+07 | 8.643E+02 |
| 2049 | 3.087E+04 | 2.472E+07 | 1.661E+03 | 8.246E+03 | 1.236E+07 | 8.305E+02 |

Results (Continued)

| Year | Total landfill gas | | | Methane | | |
|------|--------------------|------------------------|---------------------------|-----------|------------------------|---------------------------|
| | (Mg/year) | (m ³ /year) | (av ft ³ /min) | (Mg/year) | (m ³ /year) | (av ft ³ /min) |
| 2050 | 2.966E+04 | 2.375E+07 | 1.596E+03 | 7.922E+03 | 1.188E+07 | 7.979E+02 |
| 2051 | 2.850E+04 | 2.282E+07 | 1.533E+03 | 7.612E+03 | 1.141E+07 | 7.666E+02 |
| 2052 | 2.738E+04 | 2.192E+07 | 1.473E+03 | 7.313E+03 | 1.096E+07 | 7.365E+02 |
| 2053 | 2.631E+04 | 2.106E+07 | 1.415E+03 | 7.027E+03 | 1.053E+07 | 7.077E+02 |
| 2054 | 2.527E+04 | 2.024E+07 | 1.360E+03 | 6.751E+03 | 1.012E+07 | 6.799E+02 |
| 2055 | 2.428E+04 | 1.945E+07 | 1.307E+03 | 6.486E+03 | 9.723E+06 | 6.533E+02 |
| 2056 | 2.333E+04 | 1.868E+07 | 1.255E+03 | 6.232E+03 | 9.341E+06 | 6.276E+02 |
| 2057 | 2.242E+04 | 1.795E+07 | 1.206E+03 | 5.988E+03 | 8.975E+06 | 6.030E+02 |
| 2058 | 2.154E+04 | 1.725E+07 | 1.159E+03 | 5.753E+03 | 8.623E+06 | 5.794E+02 |
| 2059 | 2.069E+04 | 1.657E+07 | 1.113E+03 | 5.527E+03 | 8.285E+06 | 5.567E+02 |
| 2060 | 1.988E+04 | 1.592E+07 | 1.070E+03 | 5.311E+03 | 7.960E+06 | 5.348E+02 |
| 2061 | 1.910E+04 | 1.530E+07 | 1.028E+03 | 5.102E+03 | 7.648E+06 | 5.139E+02 |
| 2062 | 1.835E+04 | 1.470E+07 | 9.874E+02 | 4.902E+03 | 7.348E+06 | 4.937E+02 |
| 2063 | 1.763E+04 | 1.412E+07 | 9.487E+02 | 4.710E+03 | 7.060E+06 | 4.744E+02 |
| 2064 | 1.694E+04 | 1.357E+07 | 9.115E+02 | 4.525E+03 | 6.783E+06 | 4.558E+02 |
| 2065 | 1.628E+04 | 1.303E+07 | 8.758E+02 | 4.348E+03 | 6.517E+06 | 4.379E+02 |
| 2066 | 1.564E+04 | 1.252E+07 | 8.414E+02 | 4.177E+03 | 6.262E+06 | 4.207E+02 |
| 2067 | 1.503E+04 | 1.203E+07 | 8.084E+02 | 4.014E+03 | 6.016E+06 | 4.042E+02 |
| 2068 | 1.444E+04 | 1.156E+07 | 7.768E+02 | 3.856E+03 | 5.780E+06 | 3.884E+02 |
| 2069 | 1.387E+04 | 1.111E+07 | 7.463E+02 | 3.705E+03 | 5.554E+06 | 3.731E+02 |
| 2070 | 1.333E+04 | 1.067E+07 | 7.170E+02 | 3.560E+03 | 5.336E+06 | 3.585E+02 |
| 2071 | 1.280E+04 | 1.025E+07 | 6.889E+02 | 3.420E+03 | 5.127E+06 | 3.445E+02 |
| 2072 | 1.230E+04 | 9.851E+06 | 6.619E+02 | 3.286E+03 | 4.926E+06 | 3.310E+02 |
| 2073 | 1.182E+04 | 9.465E+06 | 6.359E+02 | 3.157E+03 | 4.732E+06 | 3.180E+02 |
| 2074 | 1.136E+04 | 9.094E+06 | 6.110E+02 | 3.033E+03 | 4.547E+06 | 3.055E+02 |
| 2075 | 1.091E+04 | 8.737E+06 | 5.871E+02 | 2.915E+03 | 4.369E+06 | 2.935E+02 |
| 2076 | 1.048E+04 | 8.395E+06 | 5.640E+02 | 2.800E+03 | 4.197E+06 | 2.820E+02 |
| 2077 | 1.007E+04 | 8.066E+06 | 5.419E+02 | 2.690E+03 | 4.033E+06 | 2.710E+02 |
| 2078 | 9.677E+03 | 7.749E+06 | 5.207E+02 | 2.585E+03 | 3.875E+06 | 2.603E+02 |
| 2079 | 9.298E+03 | 7.445E+06 | 5.003E+02 | 2.484E+03 | 3.723E+06 | 2.501E+02 |
| 2080 | 8.933E+03 | 7.153E+06 | 4.806E+02 | 2.386E+03 | 3.577E+06 | 2.403E+02 |
| 2081 | 8.583E+03 | 6.873E+06 | 4.618E+02 | 2.293E+03 | 3.436E+06 | 2.309E+02 |
| 2082 | 8.247E+03 | 6.603E+06 | 4.437E+02 | 2.203E+03 | 3.302E+06 | 2.218E+02 |
| 2083 | 7.923E+03 | 6.345E+06 | 4.263E+02 | 2.116E+03 | 3.172E+06 | 2.131E+02 |
| 2084 | 7.613E+03 | 6.096E+06 | 4.096E+02 | 2.033E+03 | 3.048E+06 | 2.048E+02 |
| 2085 | 7.314E+03 | 5.857E+06 | 3.935E+02 | 1.954E+03 | 2.928E+06 | 1.968E+02 |
| 2086 | 7.027E+03 | 5.627E+06 | 3.781E+02 | 1.877E+03 | 2.814E+06 | 1.890E+02 |
| 2087 | 6.752E+03 | 5.406E+06 | 3.633E+02 | 1.803E+03 | 2.703E+06 | 1.816E+02 |
| 2088 | 6.487E+03 | 5.194E+06 | 3.490E+02 | 1.733E+03 | 2.597E+06 | 1.745E+02 |
| 2089 | 6.233E+03 | 4.991E+06 | 3.353E+02 | 1.665E+03 | 2.495E+06 | 1.677E+02 |
| 2090 | 5.988E+03 | 4.795E+06 | 3.222E+02 | 1.600E+03 | 2.398E+06 | 1.611E+02 |
| 2091 | 5.753E+03 | 4.607E+06 | 3.095E+02 | 1.537E+03 | 2.304E+06 | 1.548E+02 |
| 2092 | 5.528E+03 | 4.426E+06 | 2.974E+02 | 1.477E+03 | 2.213E+06 | 1.487E+02 |
| 2093 | 5.311E+03 | 4.253E+06 | 2.858E+02 | 1.419E+03 | 2.126E+06 | 1.429E+02 |
| 2094 | 5.103E+03 | 4.086E+06 | 2.745E+02 | 1.363E+03 | 2.043E+06 | 1.373E+02 |
| 2095 | 4.903E+03 | 3.926E+06 | 2.638E+02 | 1.310E+03 | 1.963E+06 | 1.319E+02 |
| 2096 | 4.711E+03 | 3.772E+06 | 2.534E+02 | 1.258E+03 | 1.886E+06 | 1.267E+02 |
| 2097 | 4.526E+03 | 3.624E+06 | 2.435E+02 | 1.209E+03 | 1.812E+06 | 1.218E+02 |
| 2098 | 4.348E+03 | 3.482E+06 | 2.340E+02 | 1.161E+03 | 1.741E+06 | 1.170E+02 |
| 2099 | 4.178E+03 | 3.345E+06 | 2.248E+02 | 1.116E+03 | 1.673E+06 | 1.124E+02 |
| 2100 | 4.014E+03 | 3.214E+06 | 2.160E+02 | 1.072E+03 | 1.607E+06 | 1.080E+02 |

Results (Continued)

| Year | Total landfill gas | | | Methane | | |
|------|--------------------|------------------------|---------------------------|-----------|------------------------|---------------------------|
| | (Mg/year) | (m ³ /year) | (av ft ³ /min) | (Mg/year) | (m ³ /year) | (av ft ³ /min) |
| 2101 | 3.857E+03 | 3.088E+06 | 2.075E+02 | 1.030E+03 | 1.544E+06 | 1.037E+02 |
| 2102 | 3.705E+03 | 2.967E+06 | 1.994E+02 | 9.898E+02 | 1.484E+06 | 9.968E+01 |
| 2103 | 3.560E+03 | 2.851E+06 | 1.915E+02 | 9.509E+02 | 1.425E+06 | 9.577E+01 |
| 2104 | 3.421E+03 | 2.739E+06 | 1.840E+02 | 9.137E+02 | 1.370E+06 | 9.202E+01 |
| 2105 | 3.286E+03 | 2.632E+06 | 1.768E+02 | 8.778E+02 | 1.316E+06 | 8.841E+01 |
| 2106 | 3.158E+03 | 2.528E+06 | 1.699E+02 | 8.434E+02 | 1.264E+06 | 8.494E+01 |
| 2107 | 3.034E+03 | 2.429E+06 | 1.632E+02 | 8.103E+02 | 1.215E+06 | 8.161E+01 |
| 2108 | 2.915E+03 | 2.334E+06 | 1.568E+02 | 7.786E+02 | 1.167E+06 | 7.841E+01 |
| 2109 | 2.801E+03 | 2.243E+06 | 1.507E+02 | 7.480E+02 | 1.121E+06 | 7.534E+01 |
| 2110 | 2.691E+03 | 2.155E+06 | 1.448E+02 | 7.187E+02 | 1.077E+06 | 7.238E+01 |
| 2111 | 2.585E+03 | 2.070E+06 | 1.391E+02 | 6.905E+02 | 1.035E+06 | 6.954E+01 |
| 2112 | 2.484E+03 | 1.989E+06 | 1.336E+02 | 6.635E+02 | 9.945E+05 | 6.682E+01 |
| 2113 | 2.386E+03 | 1.911E+06 | 1.284E+02 | 6.374E+02 | 9.555E+05 | 6.420E+01 |
| 2114 | 2.293E+03 | 1.836E+06 | 1.234E+02 | 6.124E+02 | 9.180E+05 | 6.168E+01 |
| 2115 | 2.203E+03 | 1.764E+06 | 1.185E+02 | 5.884E+02 | 8.820E+05 | 5.926E+01 |
| 2116 | 2.117E+03 | 1.695E+06 | 1.139E+02 | 5.654E+02 | 8.474E+05 | 5.694E+01 |
| 2117 | 2.034E+03 | 1.628E+06 | 1.094E+02 | 5.432E+02 | 8.142E+05 | 5.471E+01 |
| 2118 | 1.954E+03 | 1.565E+06 | 1.051E+02 | 5.219E+02 | 7.823E+05 | 5.256E+01 |
| 2119 | 1.877E+03 | 1.503E+06 | 1.010E+02 | 5.014E+02 | 7.516E+05 | 5.050E+01 |
| 2120 | 1.804E+03 | 1.444E+06 | 9.704E+01 | 4.818E+02 | 7.221E+05 | 4.852E+01 |
| 2121 | 1.733E+03 | 1.388E+06 | 9.323E+01 | 4.629E+02 | 6.938E+05 | 4.662E+01 |
| 2122 | 1.665E+03 | 1.333E+06 | 8.958E+01 | 4.447E+02 | 6.666E+05 | 4.479E+01 |
| 2123 | 1.600E+03 | 1.281E+06 | 8.607E+01 | 4.273E+02 | 6.405E+05 | 4.303E+01 |
| 2124 | 1.537E+03 | 1.231E+06 | 8.269E+01 | 4.105E+02 | 6.154E+05 | 4.135E+01 |
| 2125 | 1.477E+03 | 1.182E+06 | 7.945E+01 | 3.944E+02 | 5.912E+05 | 3.972E+01 |
| 2126 | 1.419E+03 | 1.136E+06 | 7.633E+01 | 3.790E+02 | 5.680E+05 | 3.817E+01 |
| 2127 | 1.363E+03 | 1.092E+06 | 7.334E+01 | 3.641E+02 | 5.458E+05 | 3.667E+01 |
| 2128 | 1.310E+03 | 1.049E+06 | 7.047E+01 | 3.498E+02 | 5.244E+05 | 3.523E+01 |
| 2129 | 1.258E+03 | 1.008E+06 | 6.770E+01 | 3.361E+02 | 5.038E+05 | 3.385E+01 |
| 2130 | 1.209E+03 | 9.681E+05 | 6.505E+01 | 3.229E+02 | 4.841E+05 | 3.252E+01 |
| 2131 | 1.162E+03 | 9.302E+05 | 6.250E+01 | 3.103E+02 | 4.651E+05 | 3.125E+01 |
| 2132 | 1.116E+03 | 8.937E+05 | 6.005E+01 | 2.981E+02 | 4.468E+05 | 3.002E+01 |
| 2133 | 1.072E+03 | 8.586E+05 | 5.769E+01 | 2.864E+02 | 4.293E+05 | 2.885E+01 |
| 2134 | 1.030E+03 | 8.250E+05 | 5.543E+01 | 2.752E+02 | 4.125E+05 | 2.771E+01 |
| 2135 | 9.898E+02 | 7.926E+05 | 5.326E+01 | 2.644E+02 | 3.963E+05 | 2.663E+01 |
| 2136 | 9.510E+02 | 7.615E+05 | 5.117E+01 | 2.540E+02 | 3.808E+05 | 2.558E+01 |
| 2137 | 9.137E+02 | 7.317E+05 | 4.916E+01 | 2.441E+02 | 3.658E+05 | 2.458E+01 |
| 2138 | 8.779E+02 | 7.030E+05 | 4.723E+01 | 2.345E+02 | 3.515E+05 | 2.362E+01 |
| 2139 | 8.435E+02 | 6.754E+05 | 4.538E+01 | 2.253E+02 | 3.377E+05 | 2.269E+01 |
| 2140 | 8.104E+02 | 6.489E+05 | 4.360E+01 | 2.165E+02 | 3.245E+05 | 2.180E+01 |

Results (Continued)

| Year | Carbon dioxide | | | NMOC | | |
|------|----------------|------------------------|---------------------------|-----------|------------------------|---------------------------|
| | (Mg/year) | (m ³ /year) | (av ft ³ /min) | (Mg/year) | (m ³ /year) | (av ft ³ /min) |
| 2000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2001 | 1.308E+01 | 7.143E+03 | 4.800E-01 | 5.582E-03 | 1.557E+00 | 1.046E-04 |
| 2002 | 6.775E+02 | 3.701E+05 | 2.487E+01 | 2.892E-01 | 8.068E+01 | 5.421E-03 |
| 2003 | 1.430E+03 | 7.810E+05 | 5.248E+01 | 6.103E-01 | 1.703E+02 | 1.144E-02 |
| 2004 | 2.233E+03 | 1.220E+06 | 8.195E+01 | 9.531E-01 | 2.659E+02 | 1.787E-02 |
| 2005 | 3.126E+03 | 1.708E+06 | 1.148E+02 | 1.335E+00 | 3.723E+02 | 2.502E-02 |
| 2006 | 4.141E+03 | 2.262E+06 | 1.520E+02 | 1.768E+00 | 4.931E+02 | 3.313E-02 |
| 2007 | 4.995E+03 | 2.729E+06 | 1.833E+02 | 2.132E+00 | 5.948E+02 | 3.997E-02 |
| 2008 | 5.674E+03 | 3.100E+06 | 2.083E+02 | 2.422E+00 | 6.757E+02 | 4.540E-02 |
| 2009 | 6.317E+03 | 3.451E+06 | 2.319E+02 | 2.697E+00 | 7.523E+02 | 5.055E-02 |
| 2010 | 6.943E+03 | 3.793E+06 | 2.548E+02 | 2.964E+00 | 8.269E+02 | 5.556E-02 |
| 2011 | 7.553E+03 | 4.126E+06 | 2.773E+02 | 3.224E+00 | 8.996E+02 | 6.044E-02 |
| 2012 | 8.149E+03 | 4.452E+06 | 2.991E+02 | 3.479E+00 | 9.704E+02 | 6.520E-02 |
| 2013 | 8.729E+03 | 4.769E+06 | 3.204E+02 | 3.726E+00 | 1.040E+03 | 6.985E-02 |
| 2014 | 9.297E+03 | 5.079E+06 | 3.412E+02 | 3.969E+00 | 1.107E+03 | 7.439E-02 |
| 2015 | 9.850E+03 | 5.381E+06 | 3.616E+02 | 4.205E+00 | 1.173E+03 | 7.882E-02 |
| 2016 | 1.039E+04 | 5.677E+06 | 3.814E+02 | 4.436E+00 | 1.238E+03 | 8.315E-02 |
| 2017 | 1.092E+04 | 5.966E+06 | 4.009E+02 | 4.662E+00 | 1.301E+03 | 8.739E-02 |
| 2018 | 1.144E+04 | 6.249E+06 | 4.199E+02 | 4.883E+00 | 1.362E+03 | 9.154E-02 |
| 2019 | 1.195E+04 | 6.526E+06 | 4.385E+02 | 5.100E+00 | 1.423E+03 | 9.559E-02 |
| 2020 | 1.244E+04 | 6.798E+06 | 4.567E+02 | 5.312E+00 | 1.482E+03 | 9.957E-02 |
| 2021 | 1.293E+04 | 7.064E+06 | 4.746E+02 | 5.520E+00 | 1.540E+03 | 1.035E-01 |
| 2022 | 1.341E+04 | 7.325E+06 | 4.922E+02 | 5.724E+00 | 1.597E+03 | 1.073E-01 |
| 2023 | 1.388E+04 | 7.581E+06 | 5.094E+02 | 5.924E+00 | 1.653E+03 | 1.110E-01 |
| 2024 | 1.434E+04 | 7.832E+06 | 5.263E+02 | 6.120E+00 | 1.707E+03 | 1.147E-01 |
| 2025 | 1.479E+04 | 8.080E+06 | 5.429E+02 | 6.313E+00 | 1.761E+03 | 1.183E-01 |
| 2026 | 1.523E+04 | 8.323E+06 | 5.592E+02 | 6.503E+00 | 1.814E+03 | 1.219E-01 |
| 2027 | 1.567E+04 | 8.562E+06 | 5.753E+02 | 6.690E+00 | 1.866E+03 | 1.254E-01 |
| 2028 | 1.610E+04 | 8.797E+06 | 5.911E+02 | 6.874E+00 | 1.918E+03 | 1.289E-01 |
| 2029 | 1.653E+04 | 9.029E+06 | 6.066E+02 | 7.055E+00 | 1.968E+03 | 1.322E-01 |
| 2030 | 1.695E+04 | 9.257E+06 | 6.220E+02 | 7.234E+00 | 2.018E+03 | 1.356E-01 |
| 2031 | 1.736E+04 | 9.483E+06 | 6.371E+02 | 7.410E+00 | 2.067E+03 | 1.389E-01 |
| 2032 | 1.776E+04 | 9.705E+06 | 6.521E+02 | 7.584E+00 | 2.116E+03 | 1.422E-01 |
| 2033 | 1.817E+04 | 9.925E+06 | 6.668E+02 | 7.755E+00 | 2.164E+03 | 1.454E-01 |
| 2034 | 1.856E+04 | 1.014E+07 | 6.814E+02 | 7.925E+00 | 2.211E+03 | 1.485E-01 |
| 2035 | 1.896E+04 | 1.036E+07 | 6.958E+02 | 8.092E+00 | 2.258E+03 | 1.517E-01 |
| 2036 | 1.935E+04 | 1.057E+07 | 7.101E+02 | 8.258E+00 | 2.304E+03 | 1.548E-01 |
| 2037 | 1.973E+04 | 1.078E+07 | 7.242E+02 | 8.423E+00 | 2.350E+03 | 1.579E-01 |
| 2038 | 2.011E+04 | 1.099E+07 | 7.382E+02 | 8.585E+00 | 2.395E+03 | 1.609E-01 |
| 2039 | 2.049E+04 | 1.119E+07 | 7.521E+02 | 8.746E+00 | 2.440E+03 | 1.639E-01 |
| 2040 | 2.086E+04 | 1.140E+07 | 7.658E+02 | 8.906E+00 | 2.485E+03 | 1.669E-01 |
| 2041 | 2.123E+04 | 1.160E+07 | 7.794E+02 | 9.065E+00 | 2.529E+03 | 1.699E-01 |
| 2042 | 2.160E+04 | 1.180E+07 | 7.930E+02 | 9.222E+00 | 2.573E+03 | 1.729E-01 |
| 2043 | 2.197E+04 | 1.200E+07 | 8.064E+02 | 9.379E+00 | 2.617E+03 | 1.758E-01 |
| 2044 | 2.233E+04 | 1.220E+07 | 8.198E+02 | 9.534E+00 | 2.660E+03 | 1.787E-01 |
| 2045 | 2.270E+04 | 1.240E+07 | 8.331E+02 | 9.689E+00 | 2.703E+03 | 1.816E-01 |
| 2046 | 2.306E+04 | 1.260E+07 | 8.463E+02 | 9.843E+00 | 2.746E+03 | 1.845E-01 |
| 2047 | 2.342E+04 | 1.279E+07 | 8.595E+02 | 9.996E+00 | 2.789E+03 | 1.874E-01 |
| 2048 | 2.355E+04 | 1.286E+07 | 8.643E+02 | 1.005E+01 | 2.804E+03 | 1.884E-01 |
| 2049 | 2.262E+04 | 1.236E+07 | 8.305E+02 | 9.658E+00 | 2.694E+03 | 1.810E-01 |

Results (Continued)

| Year | Carbon dioxide | | | NMOC | | |
|------|----------------|------------------------|---------------------------|-----------|------------------------|---------------------------|
| | (Mg/year) | (m ³ /year) | (av ft ³ /min) | (Mg/year) | (m ³ /year) | (av ft ³ /min) |
| 2050 | 2.174E+04 | 1.188E+07 | 7.979E+02 | 9.279E+00 | 2.589E+03 | 1.739E-01 |
| 2051 | 2.089E+04 | 1.141E+07 | 7.666E+02 | 8.916E+00 | 2.487E+03 | 1.671E-01 |
| 2052 | 2.007E+04 | 1.096E+07 | 7.365E+02 | 8.566E+00 | 2.390E+03 | 1.606E-01 |
| 2053 | 1.928E+04 | 1.053E+07 | 7.077E+02 | 8.230E+00 | 2.296E+03 | 1.543E-01 |
| 2054 | 1.852E+04 | 1.012E+07 | 6.799E+02 | 7.907E+00 | 2.206E+03 | 1.482E-01 |
| 2055 | 1.780E+04 | 9.723E+06 | 6.533E+02 | 7.597E+00 | 2.120E+03 | 1.424E-01 |
| 2056 | 1.710E+04 | 9.341E+06 | 6.276E+02 | 7.299E+00 | 2.036E+03 | 1.368E-01 |
| 2057 | 1.643E+04 | 8.975E+06 | 6.030E+02 | 7.013E+00 | 1.957E+03 | 1.315E-01 |
| 2058 | 1.578E+04 | 8.623E+06 | 5.794E+02 | 6.738E+00 | 1.880E+03 | 1.263E-01 |
| 2059 | 1.517E+04 | 8.285E+06 | 5.567E+02 | 6.474E+00 | 1.806E+03 | 1.214E-01 |
| 2060 | 1.457E+04 | 7.960E+06 | 5.348E+02 | 6.220E+00 | 1.735E+03 | 1.166E-01 |
| 2061 | 1.400E+04 | 7.648E+06 | 5.139E+02 | 5.976E+00 | 1.667E+03 | 1.120E-01 |
| 2062 | 1.345E+04 | 7.348E+06 | 4.937E+02 | 5.742E+00 | 1.602E+03 | 1.076E-01 |
| 2063 | 1.292E+04 | 7.060E+06 | 4.744E+02 | 5.517E+00 | 1.539E+03 | 1.034E-01 |
| 2064 | 1.242E+04 | 6.783E+06 | 4.558E+02 | 5.300E+00 | 1.479E+03 | 9.936E-02 |
| 2065 | 1.193E+04 | 6.517E+06 | 4.379E+02 | 5.093E+00 | 1.421E+03 | 9.546E-02 |
| 2066 | 1.146E+04 | 6.262E+06 | 4.207E+02 | 4.893E+00 | 1.365E+03 | 9.172E-02 |
| 2067 | 1.101E+04 | 6.016E+06 | 4.042E+02 | 4.701E+00 | 1.312E+03 | 8.812E-02 |
| 2068 | 1.058E+04 | 5.780E+06 | 3.884E+02 | 4.517E+00 | 1.260E+03 | 8.467E-02 |
| 2069 | 1.017E+04 | 5.554E+06 | 3.731E+02 | 4.340E+00 | 1.211E+03 | 8.135E-02 |
| 2070 | 9.767E+03 | 5.336E+06 | 3.585E+02 | 4.170E+00 | 1.163E+03 | 7.816E-02 |
| 2071 | 9.384E+03 | 5.127E+06 | 3.445E+02 | 4.006E+00 | 1.118E+03 | 7.509E-02 |
| 2072 | 9.016E+03 | 4.926E+06 | 3.310E+02 | 3.849E+00 | 1.074E+03 | 7.215E-02 |
| 2073 | 8.663E+03 | 4.732E+06 | 3.180E+02 | 3.698E+00 | 1.032E+03 | 6.932E-02 |
| 2074 | 8.323E+03 | 4.547E+06 | 3.055E+02 | 3.553E+00 | 9.912E+02 | 6.660E-02 |
| 2075 | 7.997E+03 | 4.369E+06 | 2.935E+02 | 3.414E+00 | 9.524E+02 | 6.399E-02 |
| 2076 | 7.683E+03 | 4.197E+06 | 2.820E+02 | 3.280E+00 | 9.150E+02 | 6.148E-02 |
| 2077 | 7.382E+03 | 4.033E+06 | 2.710E+02 | 3.151E+00 | 8.791E+02 | 5.907E-02 |
| 2078 | 7.092E+03 | 3.875E+06 | 2.603E+02 | 3.028E+00 | 8.447E+02 | 5.675E-02 |
| 2079 | 6.814E+03 | 3.723E+06 | 2.501E+02 | 2.909E+00 | 8.115E+02 | 5.453E-02 |
| 2080 | 6.547E+03 | 3.577E+06 | 2.403E+02 | 2.795E+00 | 7.797E+02 | 5.239E-02 |
| 2081 | 6.290E+03 | 3.436E+06 | 2.309E+02 | 2.685E+00 | 7.492E+02 | 5.034E-02 |
| 2082 | 6.044E+03 | 3.302E+06 | 2.218E+02 | 2.580E+00 | 7.198E+02 | 4.836E-02 |
| 2083 | 5.807E+03 | 3.172E+06 | 2.131E+02 | 2.479E+00 | 6.916E+02 | 4.647E-02 |
| 2084 | 5.579E+03 | 3.048E+06 | 2.048E+02 | 2.382E+00 | 6.644E+02 | 4.464E-02 |
| 2085 | 5.360E+03 | 2.928E+06 | 1.968E+02 | 2.288E+00 | 6.384E+02 | 4.289E-02 |
| 2086 | 5.150E+03 | 2.814E+06 | 1.890E+02 | 2.199E+00 | 6.134E+02 | 4.121E-02 |
| 2087 | 4.948E+03 | 2.703E+06 | 1.816E+02 | 2.112E+00 | 5.893E+02 | 3.960E-02 |
| 2088 | 4.754E+03 | 2.597E+06 | 1.745E+02 | 2.030E+00 | 5.662E+02 | 3.804E-02 |
| 2089 | 4.568E+03 | 2.495E+06 | 1.677E+02 | 1.950E+00 | 5.440E+02 | 3.655E-02 |
| 2090 | 4.389E+03 | 2.398E+06 | 1.611E+02 | 1.873E+00 | 5.227E+02 | 3.512E-02 |
| 2091 | 4.217E+03 | 2.304E+06 | 1.548E+02 | 1.800E+00 | 5.022E+02 | 3.374E-02 |
| 2092 | 4.051E+03 | 2.213E+06 | 1.487E+02 | 1.729E+00 | 4.825E+02 | 3.242E-02 |
| 2093 | 3.892E+03 | 2.126E+06 | 1.429E+02 | 1.662E+00 | 4.636E+02 | 3.115E-02 |
| 2094 | 3.740E+03 | 2.043E+06 | 1.373E+02 | 1.596E+00 | 4.454E+02 | 2.993E-02 |
| 2095 | 3.593E+03 | 1.963E+06 | 1.319E+02 | 1.534E+00 | 4.279E+02 | 2.875E-02 |
| 2096 | 3.452E+03 | 1.886E+06 | 1.267E+02 | 1.474E+00 | 4.111E+02 | 2.762E-02 |
| 2097 | 3.317E+03 | 1.812E+06 | 1.218E+02 | 1.416E+00 | 3.950E+02 | 2.654E-02 |
| 2098 | 3.187E+03 | 1.741E+06 | 1.170E+02 | 1.360E+00 | 3.795E+02 | 2.550E-02 |
| 2099 | 3.062E+03 | 1.673E+06 | 1.124E+02 | 1.307E+00 | 3.647E+02 | 2.450E-02 |
| 2100 | 2.942E+03 | 1.607E+06 | 1.080E+02 | 1.256E+00 | 3.504E+02 | 2.354E-02 |

Results (Continued)

| Year | Carbon dioxide | | | NMOC | | |
|------|----------------|------------------------|---------------------------|-----------|------------------------|---------------------------|
| | (Mg/year) | (m ³ /year) | (av ft ³ /min) | (Mg/year) | (m ³ /year) | (av ft ³ /min) |
| 2101 | 2.826E+03 | 1.544E+06 | 1.037E+02 | 1.207E+00 | 3.366E+02 | 2.262E-02 |
| 2102 | 2.716E+03 | 1.484E+06 | 9.968E+01 | 1.159E+00 | 3.234E+02 | 2.173E-02 |
| 2103 | 2.609E+03 | 1.425E+06 | 9.577E+01 | 1.114E+00 | 3.107E+02 | 2.088E-02 |
| 2104 | 2.507E+03 | 1.370E+06 | 9.202E+01 | 1.070E+00 | 2.986E+02 | 2.006E-02 |
| 2105 | 2.409E+03 | 1.316E+06 | 8.841E+01 | 1.028E+00 | 2.868E+02 | 1.927E-02 |
| 2106 | 2.314E+03 | 1.264E+06 | 8.494E+01 | 9.879E-01 | 2.756E+02 | 1.852E-02 |
| 2107 | 2.223E+03 | 1.215E+06 | 8.161E+01 | 9.491E-01 | 2.648E+02 | 1.779E-02 |
| 2108 | 2.136E+03 | 1.167E+06 | 7.841E+01 | 9.119E-01 | 2.544E+02 | 1.709E-02 |
| 2109 | 2.052E+03 | 1.121E+06 | 7.534E+01 | 8.762E-01 | 2.444E+02 | 1.642E-02 |
| 2110 | 1.972E+03 | 1.077E+06 | 7.238E+01 | 8.418E-01 | 2.348E+02 | 1.578E-02 |
| 2111 | 1.895E+03 | 1.035E+06 | 6.954E+01 | 8.088E-01 | 2.256E+02 | 1.516E-02 |
| 2112 | 1.820E+03 | 9.945E+05 | 6.682E+01 | 7.771E-01 | 2.168E+02 | 1.457E-02 |
| 2113 | 1.749E+03 | 9.555E+05 | 6.420E+01 | 7.466E-01 | 2.083E+02 | 1.400E-02 |
| 2114 | 1.680E+03 | 9.180E+05 | 6.168E+01 | 7.173E-01 | 2.001E+02 | 1.345E-02 |
| 2115 | 1.615E+03 | 8.820E+05 | 5.926E+01 | 6.892E-01 | 1.923E+02 | 1.292E-02 |
| 2116 | 1.551E+03 | 8.474E+05 | 5.694E+01 | 6.622E-01 | 1.847E+02 | 1.241E-02 |
| 2117 | 1.490E+03 | 8.142E+05 | 5.471E+01 | 6.362E-01 | 1.775E+02 | 1.193E-02 |
| 2118 | 1.432E+03 | 7.823E+05 | 5.256E+01 | 6.113E-01 | 1.705E+02 | 1.146E-02 |
| 2119 | 1.376E+03 | 7.516E+05 | 5.050E+01 | 5.873E-01 | 1.638E+02 | 1.101E-02 |
| 2120 | 1.322E+03 | 7.221E+05 | 4.852E+01 | 5.643E-01 | 1.574E+02 | 1.058E-02 |
| 2121 | 1.270E+03 | 6.938E+05 | 4.662E+01 | 5.422E-01 | 1.513E+02 | 1.016E-02 |
| 2122 | 1.220E+03 | 6.666E+05 | 4.479E+01 | 5.209E-01 | 1.453E+02 | 9.764E-03 |
| 2123 | 1.172E+03 | 6.405E+05 | 4.303E+01 | 5.005E-01 | 1.396E+02 | 9.381E-03 |
| 2124 | 1.126E+03 | 6.154E+05 | 4.135E+01 | 4.808E-01 | 1.341E+02 | 9.013E-03 |
| 2125 | 1.082E+03 | 5.912E+05 | 3.972E+01 | 4.620E-01 | 1.289E+02 | 8.660E-03 |
| 2126 | 1.040E+03 | 5.680E+05 | 3.817E+01 | 4.439E-01 | 1.238E+02 | 8.320E-03 |
| 2127 | 9.990E+02 | 5.458E+05 | 3.667E+01 | 4.265E-01 | 1.190E+02 | 7.994E-03 |
| 2128 | 9.599E+02 | 5.244E+05 | 3.523E+01 | 4.098E-01 | 1.143E+02 | 7.681E-03 |
| 2129 | 9.222E+02 | 5.038E+05 | 3.385E+01 | 3.937E-01 | 1.098E+02 | 7.380E-03 |
| 2130 | 8.861E+02 | 4.841E+05 | 3.252E+01 | 3.782E-01 | 1.055E+02 | 7.090E-03 |
| 2131 | 8.513E+02 | 4.651E+05 | 3.125E+01 | 3.634E-01 | 1.014E+02 | 6.812E-03 |
| 2132 | 8.179E+02 | 4.468E+05 | 3.002E+01 | 3.492E-01 | 9.741E+01 | 6.545E-03 |
| 2133 | 7.859E+02 | 4.293E+05 | 2.885E+01 | 3.355E-01 | 9.359E+01 | 6.288E-03 |
| 2134 | 7.551E+02 | 4.125E+05 | 2.771E+01 | 3.223E-01 | 8.992E+01 | 6.042E-03 |
| 2135 | 7.255E+02 | 3.963E+05 | 2.663E+01 | 3.097E-01 | 8.640E+01 | 5.805E-03 |
| 2136 | 6.970E+02 | 3.808E+05 | 2.558E+01 | 2.975E-01 | 8.301E+01 | 5.577E-03 |
| 2137 | 6.697E+02 | 3.658E+05 | 2.458E+01 | 2.859E-01 | 7.975E+01 | 5.359E-03 |
| 2138 | 6.434E+02 | 3.515E+05 | 2.362E+01 | 2.747E-01 | 7.663E+01 | 5.149E-03 |
| 2139 | 6.182E+02 | 3.377E+05 | 2.269E+01 | 2.639E-01 | 7.362E+01 | 4.947E-03 |
| 2140 | 5.939E+02 | 3.245E+05 | 2.180E+01 | 2.535E-01 | 7.074E+01 | 4.753E-03 |

Closure
Cells 1 through Cells 14
Mueller Equation Calculations

JOB Forty West Landfill - At Closure

PROJECT NO.: 13813514.00001

DESCRIPTION Mueller Equation Calculation Summary

COMPUTED BY

KMC

DATE:

29-Jan-10

CHECKED BY

NSG/JDM

DATE:

18-Jan-10

| | Total Flow (scfm) | Headloss (in H ₂ O) |
|----------------------|-------------------|--------------------------------|
| North Header | 970.54 | 10.69 |
| South Header | 758.15 | 11.57 |
| Flare Station Piping | 1728.69 | 0.60 |

Total Headloss (max.)

12.17

Operational Head

10.00

Total Vacuum Required

22.17

- 1) Total Headloss (max.) is the headloss from the headers to the flare station plus the larger of the two header head loss values.
- 2) Operational head is the theoretical vacuum available at the most remote wellhead.
- 3) Headloss through the 4" lateral pipes was negligible (<0.1 inches)
- 4) System minor losses are accounted for by the pressure drop safety factor of 1.5.

JOB DESCRIPTION: Forty West Landfill, Southern Header
Mueller Equation Calcs. (Cells 10, 9, 13, 11, 14, 4, 3, 2, 1)

PROJECT NO.: 13813514.00001
 COMPUTED BY: KMC
 CHECKED BY: NSG/JDM

DATE: 29-Jan-10
 DATE: 18-Jan-10

Primary Header Pipe in Cells 5-14

| | | | |
|---|----------------------------------|--------------------------|-------------------|
| Total Header Pipe Length (Slope Adjusted) | 19,250.69 lineal feet | Node Separation CFM/Node | 263.27 feet (max) |
| Allowable Pressure Drop | 0.01 | Pipe Diameter | varies |
| Pressure Drop Safety Factor | 1.50 | Accumulated Flow | 12.00 inches |
| Cumulative Pressure Drop | 11.57 inches of H ₂ O | | 758.15 scfm |

Total Landfill Area* 189.00 acres
 Total Gas Generation 1,728.69 scfm
 Flow/ft² 0.00020998 cfm/ft²
 Gas from S Header 758.15 scfm

* Total gas generation is taken from gas generation from entire landfill at closing therefore, it will not equal to flow collected by this portion of the system as calculated below.

| Cell 10 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|---------------|-------------------------|------------------------|----------------------|-------------------------|--|-------------------------------|--------------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) - (Min. Slope used) | Gas Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | | | | | | | | | | | | |
| 10BS | 1 | 228,109.20 | 11.97 | 169.47 | 11.97 | 1.71 | 12 | 0.000001 | 0.000165 | 2.00 | 0.11 | 0.03 | 0.04 |
| 10CS | 1 | 57,027.30 | 11.97 | 190.07 | 23.95 | 2.20 | 12 | 0.000003 | 0.000619 | 2.00 | 0.21 | 0.06 | 0.06 |
| 10DS | 1 | 57,027.30 | 11.97 | 122.70 | 35.92 | 2.56 | 12 | 0.000007 | 0.000909 | 2.00 | 0.32 | 0.09 | 0.06 |
| 10ES | 1 | 57,027.30 | 11.97 | 384.19 | 47.90 | 2.84 | 12 | 0.000011 | 0.004180 | 2.00 | 0.42 | 0.13 | 0.07 |
| | | | | | | | 12 | | | 2.00 | | 0.00 | 0.08 |
| | | | | | | | 12 | | | 2.00 | | 0.00 | 0.00 |
| | | | | | | | 12 | | | 2.00 | | 0.00 | 0.00 |
| | | | | | | | 12 | | | 2.00 | | 0.00 | 0.00 |
| Totals | 4 | 228,109.20 | | 866.43 | | | | | 0.005775 | | | | |

| Cell 9 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-----------------|-------------------------|------------------------|----------------------|-------------------------|--|-------------------------------|--------------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) - (Min. Slope used) | Gas Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | | | | | | | | | | | | |
| 9AS | 1 | 192,099.60 | 10.08 | 246.38 | 57.98 | 3.05 | 12 | 0.000015 | 0.003737 | 2.00 | 0.51 | 0.15 | 0.09 |
| 9BS | 1 | 48,024.90 | 10.08 | 217.68 | 68.07 | 3.24 | 12 | 0.000020 | 0.004364 | 2.00 | 0.60 | 0.18 | 0.09 |
| 9CS | 1 | 48,024.90 | 10.08 | 338.23 | 78.15 | 3.40 | 12 | 0.000025 | 0.006622 | 2.00 | 0.69 | 0.21 | 0.10 |
| 9ES | 1 | 48,024.90 | 10.08 | 429.85 | 88.24 | 3.56 | 12 | 0.000031 | 0.013533 | 2.00 | 0.78 | 0.23 | 0.11 |
| | | | | | | | 12 | | | 2.00 | | 0.00 | 0.11 |
| | | | | | | | 12 | | | 2.00 | | 0.00 | 0.00 |
| Totals | 4 | 192,099.60 | | 1,232.14 | | | | | 0.030257 | | | | |

| Cell 13 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|---------------|-------------------------|------------------------|----------------------|-------------------------|--|-------------------------------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) - (Min. Slope used) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | | | | | | | | | | | | |
| 13AS | 1 | 19,188.18 | 4.03 | 50.13 | 92.26 | 3.62 | 12 | 0.000034 | 0.001706 | 2.00 | 0.82 | 0.24 | 0.12 |
| 13BS | 1 | 19,188.18 | 4.03 | 192.4 | 96.29 | 3.67 | 12 | 0.000037 | 0.007052 | 2.00 | 0.85 | 0.25 | 0.12 |
| | | | | | | | 12 | | | 2.00 | | 0.00 | 0.13 |
| | | | | | | | 12 | | | 2.00 | | 0.00 | 0.14 |
| | | | | | | | 12 | | | 2.00 | | 0.00 | 0.14 |
| Totals | 2 | 38,376.36 | | 242.53 | | | | | 0.008757 | | | 0.00 | |

| Cell 11 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-----------------|-------------------------|------------------------|----------------------|-------------------------|--|-------------------------------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) - (Min. Slope used) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | | | | | | | | | | | | |
| 11A | 1 | 92,608.56 | 19.45 | 50.13 | 115.74 | 3.93 | 12 | 0.000050 | 0.002530 | 2.00 | 1.02 | 0.31 | 0.15 |
| 11B | 1 | 92,608.56 | 19.45 | 306.58 | 132.19 | 4.16 | 12 | 0.000066 | 0.020270 | 2.00 | 1.20 | 0.36 | 0.15 |
| 11C | 1 | 92,608.56 | 19.45 | 214.39 | 154.63 | 4.37 | 12 | 0.000084 | 0.017907 | 2.00 | 1.37 | 0.41 | 0.15 |
| 11D | 1 | 92,608.56 | 19.45 | 396.45 | 174.08 | 4.57 | 12 | 0.000103 | 0.040690 | 2.00 | 1.54 | 0.46 | 0.16 |
| 11E | 1 | 92,608.56 | 19.45 | 267.64 | 193.52 | 4.75 | 12 | 0.000123 | 0.033024 | 2.00 | 1.71 | 0.51 | 0.16 |
| Totals | 5 | 463,042.80 | | 1,235.19 | | | | | 0.114422 | | | 0.00 | |

| Cell 14 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-----------------|-------------------------|------------------------|----------------------|-------------------------|--|-------------------------------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) - (Min. Slope used) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | | | | | | | | | | | | |
| 14A | 1 | 93,305.52 | 19.59 | 179.31 | 213.12 | 4.92 | 12 | 0.000146 | 0.026165 | 2.00 | 1.88 | 0.56 | 0.17 |
| 14B | 1 | 93,305.52 | 19.59 | 198.74 | 232.71 | 5.08 | 12 | 0.000170 | 0.033793 | 2.00 | 2.06 | 0.61 | 0.17 |
| 14C | 1 | 93,305.52 | 19.59 | 218.18 | 252.30 | 5.23 | 12 | 0.000196 | 0.042699 | 2.00 | 2.23 | 0.67 | 0.18 |
| 14D | 1 | 93,305.52 | 19.59 | 237.61 | 271.89 | 5.38 | 12 | 0.000223 | 0.052961 | 2.00 | 2.40 | 0.72 | 0.18 |
| 14E | 1 | 93,305.52 | 19.59 | 257.05 | 291.49 | 5.52 | 12 | 0.000252 | 0.064664 | 2.00 | 2.58 | 0.77 | 0.18 |
| Totals | 5 | 466,527.60 | | 1,090.89 | | | | | 0.220282 | | | 0.00 | |

| Cell 4 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-----------------|-------------------------|------------------------|----------------------|-------------------------|--|-------------------------------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) - (Min. Slope used) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | 617,245.20 | | | | | | | | | | | |
| 4A | 3 | 115,733.48 | 24.30 | 635.50 | 315.79 | 5.68 | 12 | 0.000289 | 0.183756 | 2.00 | 2.79 | 0.83 | 0.19 |
| 4B | 4 | 154,311.30 | 32.40 | 697.26 | 348.19 | 5.89 | 12 | 0.000343 | 0.238944 | 2.00 | 3.08 | 0.92 | 0.20 |
| 4C | 2 | 77,155.65 | 16.20 | 790.92 | 364.39 | 5.99 | 12 | 0.000371 | 0.293349 | 2.00 | 3.22 | 0.96 | 0.20 |
| 4D | 3 | 115,733.48 | 24.30 | 897.33 | 388.69 | 6.13 | 12 | 0.000415 | 0.289370 | 2.00 | 3.44 | 1.03 | |
| 4E | 4 | 154,311.30 | 32.40 | 836.66 | 421.09 | 6.31 | 12 | 0.000477 | 0.399081 | 2.00 | 3.72 | 1.11 | |
| Totals | 16 | 617,245.20 | | 3,657.67 | | | | | 1.404479 | | | 0.00 | |

| Cell 3 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-----------------|-------------------------|------------------------|----------------------|-------------------------|--|-------------------------------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) - (Min. Slope used) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | 634,233.60 | | | | | | | | | | | |
| 3A | 3 | 90,604.80 | 19.03 | 740.41 | 440.12 | 6.42 | 12 | 0.000515 | 0.381364 | 2.00 | 3.89 | 1.16 | |
| 3B | 4 | 120,806.40 | 25.37 | 686.75 | 465.49 | 6.55 | 12 | 0.000568 | 0.389933 | 2.00 | 4.12 | 1.23 | |
| 3C | 3 | 90,604.80 | 19.03 | 647.40 | 484.51 | 6.65 | 12 | 0.000609 | 0.394112 | 2.00 | 4.28 | 1.28 | |
| 3D | 4 | 120,806.40 | 25.37 | 694.56 | 509.88 | 6.77 | 12 | 0.000665 | 0.462062 | 2.00 | 4.51 | 1.35 | |
| 3E | 3 | 90,604.80 | 19.03 | 647.88 | 528.90 | 6.87 | 12 | 0.000709 | 0.459362 | 2.00 | 4.68 | 1.40 | |
| 3F | 4 | 120,806.40 | 25.37 | 609.78 | 554.27 | 6.98 | 12 | 0.000769 | 0.469047 | 2.00 | 4.90 | 1.46 | |
| Totals | 21 | 634,233.60 | | 3,417.00 | 554.27 | | | | 2.553879 | | | 0.00 | |

| Cell 2 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-----------------|-------------------------|------------------------|----------------------|-------------------------|--|-------------------------------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) - (Min. Slope used) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | 470,448.00 | | | | | | | | | | | |
| 2A | 3 | 88,209.00 | 18.52 | 723.34 | 572.79 | 7.07 | 12 | 0.000814 | 0.589132 | 2.00 | 5.06 | 1.51 | |
| 2B | 4 | 117,612.00 | 24.70 | 675.28 | 597.49 | 7.18 | 12 | 0.000876 | 0.591884 | 2.00 | 5.28 | 1.58 | |
| 2C | 2 | 58,806.00 | 12.35 | 780.61 | 609.84 | 7.23 | 12 | 0.000908 | 0.708985 | 2.00 | 5.39 | 1.61 | |
| 2D | 3 | 88,209.00 | 18.52 | 904.17 | 628.36 | 7.31 | 12 | 0.000957 | 0.865071 | 2.00 | 5.56 | 1.66 | |
| 2E | 4 | 117,612.00 | 24.70 | 991.07 | 653.06 | 7.42 | 12 | 0.001023 | 1.013964 | 2.00 | 5.77 | 1.72 | |
| Totals | 16 | 470,448.00 | | 4,074.47 | 653.06 | | | | 3.769036 | | | 0.00 | |

| Cell 1 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-----------------|-------------------------|------------------------|----------------------|-------------------------|--|-------------------------------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) - (Min. Slope used) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | 500,504.40 | | | | | | | | | | | |
| 1A | 5 | 192,501.69 | 40.42 | 1,157.17 | 693.48 | 7.58 | 12 | 0.001136 | 1.314242 | 2.00 | 6.13 | 1.83 | |
| 1B | 5 | 192,501.69 | 40.42 | 878.20 | 739.90 | 7.74 | 12 | 0.001253 | 1.100680 | 2.00 | 6.49 | 1.94 | |
| 1C | 3 | 115,501.02 | 24.25 | 785.38 | 758.15 | 7.83 | 12 | 0.001326 | 1.041607 | 2.00 | 6.70 | 2.00 | |
| Totals | 13 | 500,504.40 | | 2,820.75 | 758.15 | | | | 3.456529 | | | 0.00 | |

11.57

18.637.07

86 3,610,586.76

758.15

JOB DESCRIPTION **Forty West Landfill, Northern Header**
Mueller Equation Calcs. (Cells 10, 9, 13, 12, 8, 5, 6, 7)

PROJECT NO.: 13813514.00001
 COMPUTED BY: KMC
 CHECKED BY: NSG/JDM

DATE: 29-Jan-10
 DATE: 18-Jan-10

| | | | |
|---|----------------------------------|------------------|-------------------|
| Total Header Pipe Length (Slope Adjusted) | 13,525.02 lineal feet | Node Separation | 263.27 feet (max) |
| Allowable Pressure Drop | 0.01 | CFM/Node | varies |
| Pressure Drop Safety Factor | 1.50 | Pipe Diameter | 12.00 inches |
| Cumulative Pressure Drop | 10.69 inches of H ₂ O | Accumulated Flow | 970.54 scfm |

Total Landfill Area* 189.00 acres
 Total Gas Generation* 1,728.69 scfm
 Flow/ft² 0.00020998 cfm/ft²

Gas from N Header 970.54 scfm

* Total gas generation is taken from gas generation from entire landfill at closing therefore, it will not equal to flow collected by this portion of the system as calculated below.

| Cell 10 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-------------------------|--|-----------|--------------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) | Gas Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | 456,446.51 | | | | | | | | | | | |
| 10AN | 1 | 76,074.42 | 15.97 | 256.11 | 15.97 | 1.90 | 12 | 0.000002 | 0.000413 | 2.00 | 0.14 | 0.04 | 0.04 |
| 10BN | 1 | 76,074.42 | 15.97 | 324.04 | 31.95 | 2.45 | 12 | 0.000005 | 0.001743 | 2.00 | 0.28 | 0.08 | 0.06 |
| 10CN | 1 | 76,074.42 | 15.97 | 641.10 | 47.92 | 2.84 | 12 | 0.000011 | 0.006982 | 2.00 | 0.42 | 0.13 | 0.07 |
| 10DN | 1 | 76,074.42 | 15.97 | 448.87 | 63.90 | 3.16 | 12 | 0.000018 | 0.008062 | 2.00 | 0.56 | 0.17 | 0.08 |
| 10EN | 1 | 76,074.42 | 15.97 | 363.41 | 79.87 | 3.43 | 12 | 0.000026 | 0.009622 | 2.00 | 0.71 | 0.21 | 0.09 |
| 10FN | 1 | 76,074.42 | 15.97 | 372.67 | 95.84 | 3.67 | 12 | 0.000036 | 0.013548 | 2.00 | 0.85 | 0.25 | 0.10 |
| Totals | 6 | 456,446.51 | | 2,406.20 | | | 12 | | 0.040369 | | | 0.00 | |

| Cell 9 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-------------------------|--|-----------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | 576,298.80 | | | | | | | | | | | |
| 9A | 1 | 115,259.76 | 24.20 | 581.18 | 120.05 | 3.98 | 12 | 0.000054 | 0.031255 | 2.00 | 1.06 | 0.32 | 0.11 |
| 9B | 1 | 115,259.76 | 24.20 | 425.49 | 144.25 | 4.26 | 12 | 0.000074 | 0.031494 | 2.00 | 1.28 | 0.38 | 0.12 |
| 9C | 1 | 115,259.76 | 24.20 | 551.89 | 168.45 | 4.51 | 12 | 0.000097 | 0.053498 | 2.00 | 1.49 | 0.44 | 0.13 |
| 9D | 1 | 115,259.76 | 24.20 | 429.85 | 192.65 | 4.74 | 12 | 0.000122 | 0.052625 | 2.00 | 1.70 | 0.51 | 0.14 |
| 9E | 1 | 115,259.76 | 24.20 | | 216.86 | 4.95 | 12 | 0.000150 | | 2.00 | 1.92 | 0.57 | 0.14 |
| Totals | 5 | 576,298.80 | | 1,988.41 | | | 12 | | 0.168872 | | | 0.00 | |

| Cell 13 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-------------------------|--|-----------|----------------|----------------------------------|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) | Velocity (fps) | Accumulated Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | 729,150.84 | | | | | | | | | | | |
| 13A | 1 | 243,050.28 | 51.04 | 540.65 | 267.89 | 5.35 | 12 | 0.000217 | 0.117438 | 2.00 | 2.37 | 0.71 | 0.15 |
| 13B | 1 | 243,050.28 | 51.04 | 388.81 | 318.93 | 5.70 | 12 | 0.000294 | 0.114377 | 2.00 | 2.82 | 0.84 | 0.16 |
| 13C | 1 | 243,050.28 | 51.04 | 528.29 | 369.96 | 6.02 | 12 | 0.000381 | 0.201181 | 2.00 | 3.27 | 0.98 | 0.17 |
| | | - | - | - | - | - | 12 | - | - | 2.00 | - | 0.00 | - |
| | | - | - | - | - | - | 12 | - | - | 2.00 | - | 0.00 | - |
| | | - | - | - | - | - | 12 | - | - | 2.00 | - | 0.00 | - |
| Totals | 3 | 729,150.84 | | 1,457.75 | | | | | 0.432995 | | | | |

| Cell 12 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-------------------------|--|-----------|----------------|----------------------------------|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) | Velocity (fps) | Accumulated Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | 694,346.40 | | | | | | | | | | | |
| 12A | 1 | 231,448.80 | 48.60 | 348.09 | 418.56 | 6.30 | 12 | 0.000472 | 0.164296 | 2.00 | 3.70 | 1.11 | 0.18 |
| 12B | 1 | 231,448.80 | 48.60 | 568.79 | 467.16 | 6.56 | 12 | 0.000571 | 0.324981 | 2.00 | 4.13 | 1.23 | 0.18 |
| 12C | 1 | 231,448.80 | 48.60 | 342.53 | 515.76 | 6.80 | 12 | 0.000679 | 0.232464 | 2.00 | 4.56 | 1.36 | 0.19 |
| | | - | - | - | - | - | 12 | - | - | 2.00 | - | 0.00 | - |
| | | - | - | - | - | - | 12 | - | - | 2.00 | - | 0.00 | - |
| | | - | - | - | - | - | 12 | - | - | 2.00 | - | 0.00 | - |
| Totals | 3 | 694,346.40 | | 1,259.41 | | | | | 0.721741 | | | | |

| Cell 8 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-------------------------|--|-----------|----------------|----------------------------------|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) | Velocity (fps) | Accumulated Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | 723,096.00 | | | | | | | | | | | |
| 8A | 1 | 180,774.00 | 37.96 | 446.19 | 553.72 | 6.98 | 12 | 0.000768 | 0.342621 | 2.00 | 4.90 | 1.46 | 0.20 |
| 8B | 1 | 180,774.00 | 37.96 | 338.83 | 591.68 | 7.15 | 12 | 0.000862 | 0.291981 | 2.00 | 5.23 | 1.56 | 0.20 |
| 8C | 1 | 180,774.00 | 37.96 | 397.85 | 629.64 | 7.32 | 12 | 0.000960 | 0.381995 | 2.00 | 5.57 | 1.66 | 0.20 |
| 8D | 1 | 180,774.00 | 37.96 | 298.83 | 667.60 | 7.48 | 12 | 0.001063 | 0.317671 | 2.00 | 5.90 | 1.76 | 0.21 |
| | | - | - | - | - | - | 12 | - | - | 2.00 | - | 0.00 | - |
| | | - | - | - | - | - | 12 | - | - | 2.00 | - | 0.00 | - |
| Totals | 4 | 723,096.00 | | 1,481.70 | | | | | 1.334268 | | | | |

| Cell 5 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-------------------------|--|-----------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | | | | | | | | | | | | |
| SA | 1 | 607,226.40 | 25.50 | 355.56 | 693.10 | 7.58 | 12 | 0.001134 | 0.403440 | 2.00 | 6.13 | 1.83 | 0.21 |
| SB | 1 | 121,445.28 | 25.50 | 229.92 | 718.60 | 7.68 | 12 | 0.001208 | 0.277801 | 2.00 | 6.35 | 1.90 | 0.21 |
| SC | 1 | 121,445.28 | 25.50 | 407.88 | 744.10 | 7.78 | 12 | 0.001284 | 0.523634 | 2.00 | 6.58 | 1.97 | 0.22 |
| SD | 1 | 121,445.28 | 25.50 | 334.32 | 769.60 | 7.88 | 12 | 0.001361 | 0.455102 | 2.00 | 6.80 | 2.03 | 0.22 |
| SE | 1 | 121,445.28 | 25.50 | 289.68 | 795.10 | 7.97 | 12 | 0.001440 | 0.417336 | 2.00 | 7.03 | 2.10 | 0.22 |
| Totals | 5 | 607,226.40 | - | 1,617.36 | - | - | - | - | 2,077,313 | - | - | 0.00 | - |

| Cell 6 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-------------------------|--|-----------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | | | | | | | | | | | | |
| 6A | 1 | 474,368.40 | 19.92 | 400.20 | 815.02 | 8.05 | 12 | 0.001504 | 0.601916 | 2.00 | 7.21 | 2.15 | 0.23 |
| 6B | 1 | 94,873.68 | 19.92 | 259.48 | 834.95 | 8.12 | 12 | 0.001588 | 0.407007 | 2.00 | 7.38 | 2.21 | 0.23 |
| 6C | 1 | 94,873.68 | 19.92 | 350.55 | 854.87 | 8.19 | 12 | 0.001634 | 0.572872 | 2.00 | 7.56 | 2.26 | 0.23 |
| 6D | 1 | 94,873.68 | 19.92 | 241.22 | 874.79 | 8.26 | 12 | 0.001701 | 0.410318 | 2.00 | 7.73 | 2.31 | 0.23 |
| 6E | 1 | 94,873.68 | 19.92 | 369.39 | 894.71 | 8.33 | 12 | 0.001769 | 0.653431 | 2.00 | 7.91 | 2.36 | 0.24 |
| Totals | 5 | 474,368.40 | - | 1,620.84 | - | - | - | - | 2,645,544 | - | - | 0.00 | - |

| Cell 7 | | | | | | | | | | | | | |
|---------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-------------------------|--|-----------|----------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) | Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| EFFECTIVE CELL AREA | | | | | | | | | | | | | |
| 7A | 1 | 361,112.40 | 18.96 | 290.68 | 913.67 | 8.39 | 12 | 0.001834 | 0.533292 | 2.00 | 8.08 | 2.41 | 0.24 |
| 7B | 1 | 90,278.10 | 18.96 | 664.87 | 932.62 | 8.45 | 12 | 0.001901 | 1.264145 | 2.00 | 8.25 | 2.46 | 0.24 |
| 7C | 1 | 90,278.10 | 18.96 | 368.48 | 951.58 | 8.52 | 12 | 0.001969 | 0.726559 | 2.00 | 8.41 | 2.51 | 0.24 |
| 7D | 1 | 90,278.10 | 18.96 | 366.62 | 970.54 | 8.58 | 12 | 0.002037 | 0.747090 | 2.00 | 8.58 | 2.56 | 0.24 |
| Totals | 4 | 361,112.40 | - | 1,690.65 | - | - | - | - | 3,270,087 | - | - | - | - |

| | | | | | | | | | | | | | |
|-------------------|----|--------------|--------|-----------|--------|---|---|---|-------|---|---|---|---|
| Cumulative Total: | 35 | 4,622,045.75 | 970.54 | 13,522.32 | 970.54 | - | - | - | 10.69 | - | - | - | - |
|-------------------|----|--------------|--------|-----------|--------|---|---|---|-------|---|---|---|---|

JOB DESCRIPTION Forty West Landfill, Worst Case Lateral
Mueller Equation Calcs. (PIPE TO FLARE STATION)

PROJECT NO.: 13813514.00001
 COMPUTED BY KMC
 CHECKED BY NSG/JDM

DATE: 29-Jan-10
 DATE:

The worst case lateral calculation is intended to ensure that the dimensions specified for the entire system is properly sized to accommodate the losses from the farthest well from the blower.

SUMMARY OF RESULTS FOR PIPE TO FLARE STATION

| | |
|-----------------------------|------|
| Allowable Pressure Drop | 0.01 |
| Pressure Drop Safety Factor | 1.50 |

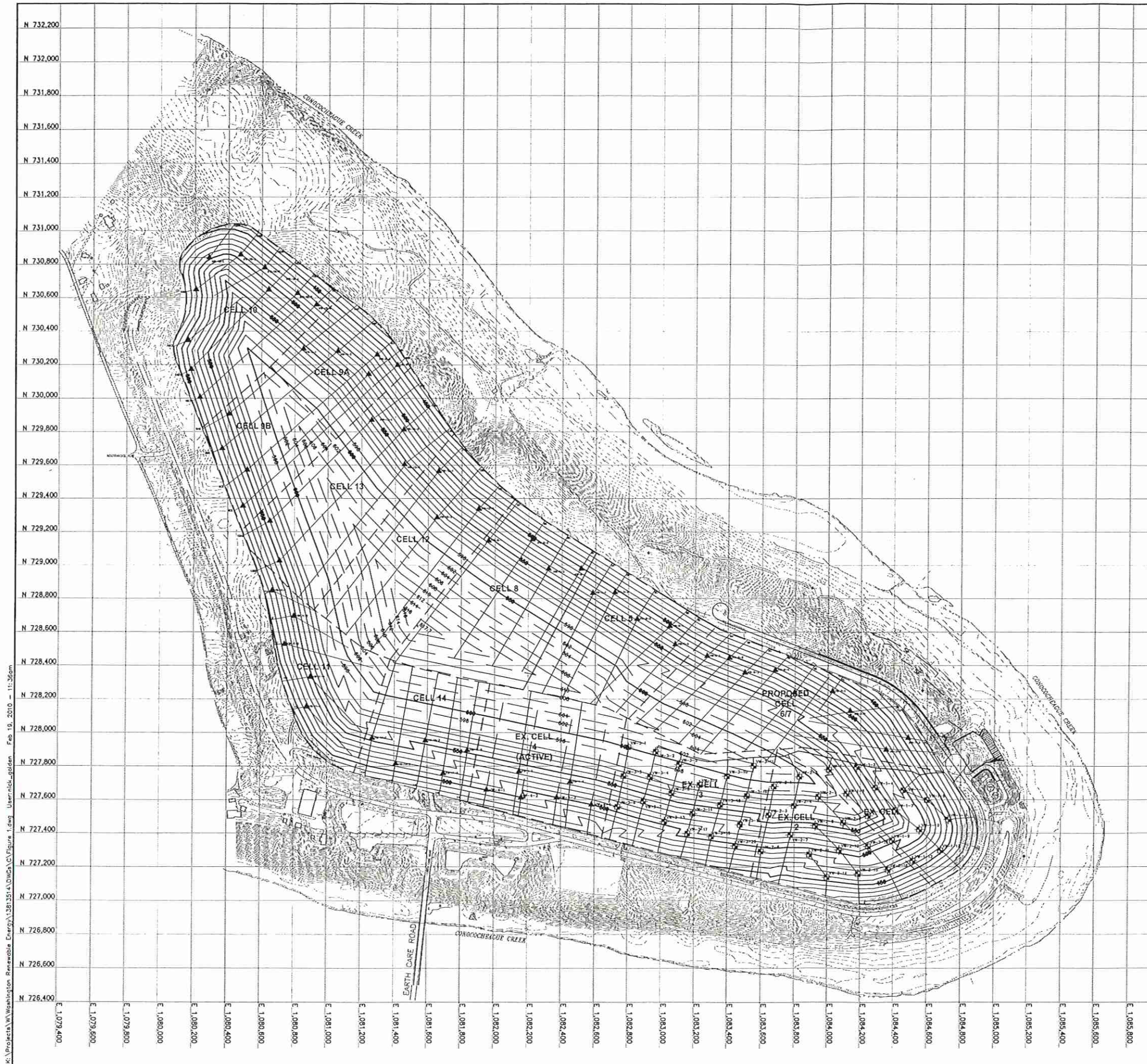
Total Landfill Area* 188.99 acres
 Total Gas Generation 1,728.69 scfm**
 Flow/ft² 0.000209986 cfm/ft²

Gas from N Header 970.54 scfm
 Gas from S Header 758.15 scfm
 Total Gas Collected 1,728.69 scfm

8,232,404.40 ft²

| Pipe to Flare Station | | | | | | | | | | | | | |
|-----------------------|------------|-------------------------|---------------------|-------------|-------------------------|------------------------|----------------------|-----------------------------|--|-----------|--------------------|---|-----------------------|
| Node ID | # of Wells | Area (ft ²) | Maximum Flow (scfm) | Length (LF) | Accumulated Flow (scfm) | Required Diameter (in) | Actual Diameter (in) | Max Actual Pressure Drop/ft | Actual Pressure Drop (in H ₂ O) | Slope (%) | Gas Velocity (fps) | Accumulated Condensate Production (gal/min) | Condensate Depth (in) |
| Pipe to Flare | n/a | n/a | n/a | 311.12 | 1,728.69 | 10.60 | 15 | 0.001931 | 0.601890 | 6.00 | 9.78 | 4.57 | |

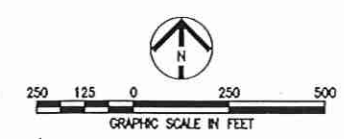
Figure 1



K:\Projects\Washington Renewable Energy\13813514\DWG\A\Figure 1.dwg User:rick_galden Feb 19, 2010 11:36am



| | | | | |
|-------------------------|---------------|------|------|----|
| ISSUED FOR BIDDING | | | DATE | BY |
| ADDENDUM REVISIONS | | | | |
| ADDENDUM NO. | ADDENDUM DATE | BY | | |
| | | | | |
| | | | | |
| | | | | |
| ISSUED FOR CONSTRUCTION | | | DATE | BY |
| CONSTRUCTION REVISIONS | | | | |
| NO. | DESCRIPTION | DATE | BY | |
| | | | | |
| | | | | |
| RECORD DRAWINGS | | | | |
| | | | | |



- GENERAL NOTES:
- EXISTING TOPOGRAPHY IS BASED UPON AERIAL PHOTOGRAMMETRY PROVIDED BY AERO-METRIC (JANUARY 2009).
 - GRID IS BASED ON MARYLAND STATE PLANE COORDINATE SYSTEM, NAD 1983. VERTICAL DATUM IS NAVD 1988.
 - THE FORTY WEST LANDFILL IS AN ACTIVE LANDFILL. THE CONTRACTOR AND ALL SUBCONTRACTORS SHALL FOLLOW ALL POSTED SPEED LIMITS AND SHALL PROVIDE A SAFE ENVIRONMENT FOR SOLID WASTE PERSONNEL, GENERAL PUBLIC AND EMPLOYEES.

COPYRIGHT: ALL RIGHTS RESERVED.

| | |
|------------------|---------------------|
| DRAWN BY: KMC | DATE: 02-19-10 |
| CHECKED BY: NSG | PROJECT #: 13813514 |
| APPROVED BY: JDM | SCALE: AS SHOWN |

GRAPHIC SCALE

WASHINGTON RENEWABLE ENERGY, LLC
 LANDFILL GAS COLLECTION SYSTEM DESIGN
 FOR EXISTING CELLS 1-4

PROPOSED LANDFILL GAS COLLECTION SYSTEM CALCULATIONS

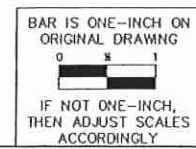


Figure 1

Stage 1 Gas Well Schedule



| WELL/FLARE ID: | LOCATION OF WELL (CELL NUMBER) | COORDINATES | | SOLID PIPE LENGTH (FT.) | SCREEN LENGTH (FT.) |
|----------------------|--------------------------------|-------------|---------|-------------------------|---------------------|
| | | NORTHING | EASTING | | |
| GAS EXTRACTION WELLS | | | | | |
| VW-1-1 | CELL 1 | 727778.56 | 1 | 10 | 20 |
| VW-1-3 | CELL 1 | 727636.01 | 1 | 10 | 32 |
| VW-1-4 | CELL 1 | 727672.01 | 1 | 10 | 18 |
| VW-1-5 | CELL 1 | 727720.00 | 1 | 10 | 14 |
| VW-1-6 | CELL 1 | 727505.05 | 1 | 10 | 31 |
| VW-1-7 | CELL 1 | 727538.93 | 1 | 10 | 35 |
| VW-1-8 | CELL 1 | 727597.18 | 1 | 10 | 31 |
| VW-1-9 | CELL 1 | 727358.05 | 1 | 10 | 40 |
| VW-1-10 | CELL 1 | 727422.24 | 1 | 10 | 44 |
| VW-1-11 | CELL 1 | 727481.79 | 1 | 10 | 21 |
| VW-1-12 | CELL 1 | 727236.18 | 1 | 10 | 38 |
| VW-1-13 | CELL 1 | 727298.24 | 1 | 10 | 26 |
| VW-2-1 | CELL 2 | 727678.73 | 1 | 10 | 38 |
| VW-2-2 | CELL 2 | 727736.71 | 1 | 10 | 34 |
| VW-2-3 | CELL 2 | 727508.50 | 1 | 10 | 45 |
| VW-2-4 | CELL 2 | 727562.46 | 1 | 10 | 44 |
| VW-2-5 | CELL 2 | 727617.23 | 1 | 10 | 38 |
| VW-2-6 | CELL 2 | 727334.00 | 1 | 10 | 25 |
| VW-2-7 | CELL 2 | 727388.96 | 1 | 10 | 51 |
| VW-2-8 | CELL 2 | 727445.46 | 1 | 10 | 38 |
| VW-2-9 | CELL 2 | 727463.73 | 1 | 10 | 28 |
| VW-2-11 | CELL 2 | 727272.96 | 1 | 10 | 35 |
| VW-2-12 | CELL 2 | 727300.46 | 1 | 10 | 34 |
| VW-2-13 | CELL 2 | 727322.89 | 1 | 10 | 32 |
| VW-2-14 | CELL 2 | 727137.96 | 1 | 10 | 10 |
| VW-2-15 | CELL 2 | 727158.96 | 1 | 10 | 24 |
| VW-2-16 | CELL 2 | 727182.96 | 1 | 10 | 32 |
| VW-3-2 | CELL 3 | 727923.67 | 1 | 10 | 18 |
| VW-3-4 | CELL 3 | 727750.91 | 1 | 10 | 24 |
| VW-3-5 | CELL 3 | 727810.00 | 1 | 10 | 23 |
| VW-3-8 | CELL 3 | 727638.00 | 1 | 10 | 23 |
| VW-3-9 | CELL 3 | 727689.00 | 1 | 10 | 27 |
| VW-3-10 | CELL 3 | 727741.50 | 1 | 10 | 31 |
| VW-3-11 | CELL 3 | 727802.71 | 1 | 10 | 12 |
| VW-3-13 | CELL 3 | 727469.00 | 1 | 10 | 16 |
| VW-3-14 | CELL 3 | 727517.50 | 1 | 10 | 32 |
| VW-3-15 | CELL 3 | 727570.50 | 1 | 10 | 33 |
| VW-3-16 | CELL 3 | 727623.80 | 1 | 10 | 35 |
| VW-3-17 | CELL 3 | 727348.24 | 1 | 10 | 15 |
| VW-3-18 | CELL 3 | 727396.50 | 1 | 10 | 22 |
| VW-3-19 | CELL 3 | 727452.80 | 1 | 10 | 40 |
| VW-3-20 | CELL 3 | 727278.80 | 1 | 10 | 22 |

Note:
 1. BASED ON TOP OF FINAL GRADE OF WASTE.
 2. BASED ON AS-BUILT TOPO OF TOP OF LCS PROVIDED
 3. EXTENDED OR NESTED WELLS TO BE INSTALLED UPO